



Short communication

# Temperature stable high K microwave dielectric ceramics of $\text{Bi}_3\text{NbO}_7$ doped by $\text{V}_2\text{O}_5$

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Received 15 September 2014; received in revised form 24 November 2014; accepted 4 December 2014

Available online 13 December 2014

## Abstract

Low firing microwave dielectric ceramics  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3,$  and  $0.5$ ) were prepared by the solid state reaction method. Sintering behavior, crystalline structure, microstructure, and microwave dielectric properties were studied. Temperature stable low-firing microwave dielectric ceramics with high permittivity were obtained in the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  system when  $x=0.1$  and  $0.2$ . The  $\text{Bi}_3(\text{Nb}_{0.9}\text{V}_{0.1})\text{O}_7$  and  $\text{Bi}_3(\text{Nb}_{0.8}\text{V}_{0.2})\text{O}_7$  ceramics sintered at  $870^\circ\text{C}$  for 2 h were found to possess high permittivity of 80 and 76, Qf (quality factor) values of 615 and 460 GHz, and TCF (temperature coefficient of frequency) values of  $-22$  and  $+3.3$  ppm/ $^\circ\text{C}$ , respectively.

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Keywords: Sintering; Dielectric properties; Capacitors

## 1. Introduction

Modern communication systems have moved to the microwave (MW) frequency region, where advanced dielectric ceramics are frequently used in resonators and filters. Miniaturization requires high relative permittivity ( $\epsilon_r$ ) materials (since the size of resonators is inversely proportional to  $\sqrt{\epsilon_r}$ ) with a near zero temperature coefficient of resonance frequency (TCF value). Furthermore, ceramics with low dielectric loss (high Qf value) are needed for the high selectivity and optimized bandwidth of the filters. More recently, by applying low-temperature co-fired ceramic (LTCC) technology, passive elements have been integrated in monolithic, highly reliable, and robust LTCC modules that consist of several layers of ceramic substrates with integrated elements (inductors, capacitors, resonators), which are interconnected with three-dimensional strip-line circuitry [1]. Microwave dielectric ceramics with high permittivity ( $\epsilon_r > 80$ ) has been widely studied [2–8], such as  $\text{Ba}_{6-3x}\text{Ln}_{8+2x}\text{Ti}_{18}\text{O}_{54}$ ,  $\text{Bi}_2\text{O}_3\text{-TiO}_2$ ,

$\text{CaTiO}_3\text{-Li}_{1/2-3x}\text{Sm}_{1/2+x}\text{TiO}_3$  system, while most of them need high sintering temperatures ( $> 1100^\circ\text{C}$ ). The  $\text{Bi}_3\text{NbO}_7$  ceramics possess low sintering temperature and good microwave dielectric properties and have attracted much attention in recent years. Valant et al. studied microwave dielectric properties of the  $\text{Bi}_3\text{NbO}_7$  ceramics and found that the cubic  $\text{Bi}_3\text{NbO}_7$  (permittivity of 100, Qf=300 GHz, TCF= $-200$  ppm/ $^\circ\text{C}$ ) and tetragonal  $\text{Bi}_3\text{NbO}_7$  (permittivity of 91, Qf=730 GHz, TCF= $+100$  ppm/ $^\circ\text{C}$ ) did not react with Ag electrode [9–12], and they were suitable for LTCC modules and microwave application if their TCF value could be modified to near zero.

The quinquevalent ion  $\text{V}^{5+}$  substitution for  $\text{Nb}^{5+}$  has improved the sintering behaviors and microwave dielectric properties of some typical Nb-based microwave dielectrics, such as  $\text{BiNbO}_4$  [13] and  $\text{LiNb}_{0.6}\text{Ti}_{0.5}\text{O}_3$  [14]. In addition, based on the similarity of chemical properties with  $\text{V}^{5+}$  and  $\text{Nb}^{5+}$ , it can be anticipated that  $\text{V}^{5+}$  substitution for  $\text{Nb}^{5+}$  might be a good choice to improve the sintering behavior and microwave dielectric properties of  $\text{Bi}_3\text{NbO}_7$  compound. In the present work,  $\text{V}_2\text{O}_5$ -doped  $\text{Bi}_3\text{NbO}_7$  compounds, that is,  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3,$  and  $0.5$ ), were prepared by solid state reaction method. The sintering behavior,

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phase structure, microstructure, and microwave dielectric properties of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3$  and  $0.5$ ) ceramics were studied.

## 2. Experimental procedure

Proportionate amounts of reagent-grade starting materials of  $\text{Bi}_2\text{O}_3$  (> 99%, Shu-Du Powders Co. Ltd, China),  $\text{Nb}_2\text{O}_5$  (> 99%, Zhu-Zhou Harden Alloys Co, Ltd, China) and  $\text{V}_2\text{O}_5$  (> 99%, Zhu-Zhou Harden Alloys Co, Ltd, China) were mixed according to the composition  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3$ , and  $0.5$ ) and ball-milled for 5 h using a planetary mill (Nanjing Machine Factory, Nanjing, China) with zirconia balls (2 mm in diameter) and alcohol as milling media. Subsequently, the mixtures were dried at  $105^\circ\text{C}$  and calcined at  $700^\circ\text{C}$  for 4 h to obtain the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  compounds. Then, the compounds were re-milled for 5 h with Zirconia balls and deionized water. After being dried, the compounds were granulated into pellets with PVA binder and pressed into cylinders (10 mm in diameter and  $4\sim 5$  mm in height) in a steel die under uniaxial pressure of  $20\text{ kN/cm}^2$ . Then the cylinder samples were sintered from  $810$  to  $990^\circ\text{C}$  for 2 h.

Crystalline structures of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  samples were investigated using X-ray diffraction with  $\text{Cu K}\alpha$  radiation (Rigaku D/MAX-2400 X-ray diffractometry, Japan). The densities of sintered specimens, as a function of sintering temperature, were measured by the liquid displacement method using deionized water as the liquid (Archimedes method). To investigate the morphology of samples, as-fired surface of sintered specimens were observed by scanning electron microscopy (SEM) (JEOL JSM-6460, Japan). Microwave dielectric properties were measured by the  $\text{TE}_{016}$  shielded cavity method with a network analyzer (8720ES, Agilent, Palo Alto, CA). The temperature coefficients of resonant frequency (TCF) were measured with the 8720ES network analyzer and a DELTA 9023 temperature chamber (Delta Design, Poway, CA) using the  $\text{TE}_{016}$  shielded cavity method. The TCF value was calculated by the following formula:

$$\text{TCF} = \frac{f_{85} - f_{25}}{f_{25} \times (85 - 25)} \text{ppm}/^\circ\text{C} \quad (1)$$

where  $f_{85}$ ,  $f_{25}$  were the  $\text{TE}_{016}$  resonant frequencies at the measuring temperature  $85^\circ\text{C}$  and at room temperature ( $25^\circ\text{C}$ ) respectively.

## 3. Results and discussion

Room temperature X-ray diffraction patterns of the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3$ , and  $0.5$ ) ceramics sintered at  $900^\circ\text{C}$  for 2 h are shown in Fig. 1. Pure  $\text{Bi}_3\text{NbO}_7$  crystallize in a cubic structure after being sintered at  $900^\circ\text{C}$  and this result corresponds well with literatures' reports [10–12]. The  $\text{Bi}_3(\text{Nb}_{0.9}\text{V}_{0.1})\text{O}_7$  and  $\text{Bi}_3(\text{Nb}_{0.8}\text{V}_{0.2})\text{O}_7$  ceramics crystallize in a tetragonal structure, as shown in Fig. 1. It indicates that V substitution for Nb in the  $\text{Bi}_3\text{NbO}_7$  ceramic led the composition to crystallize in a tetragonal phase. The cell

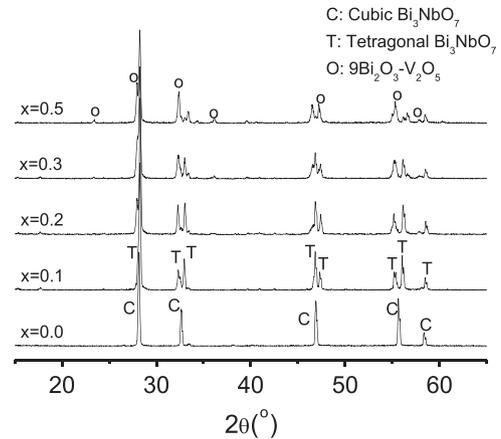


Fig. 1. X-ray diffraction patterns of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3$ , and  $0.5$ ) ceramics sintered at  $900^\circ\text{C}$  for 2 h.

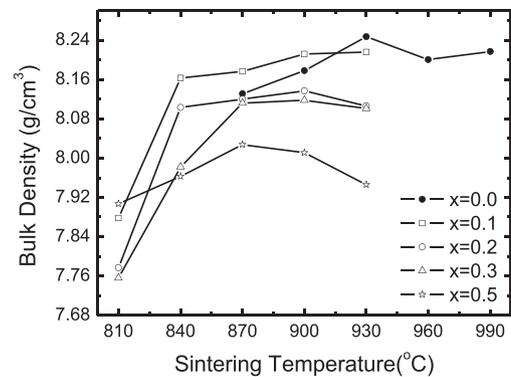


Fig. 2. Bulk densities of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3$ , and  $0.5$ ) ceramics as a function of sintering temperature.

parameters of  $\text{Bi}_3(\text{Nb}_{0.9}\text{V}_{0.1})\text{O}_7$  are  $a=b=5.430\text{ \AA}$ ,  $c=5.524\text{ \AA}$ ,  $\alpha=\beta=\gamma=90^\circ$  (cell parameter of cubic  $\text{Bi}_3\text{NbO}_7$  are  $a=b=c=5.478\text{ \AA}$ ). When the content of V substitution increased to 30 mol% ( $x=0.3$ ), Bi-rich phase of  $9\text{Bi}_2\text{O}_3\cdot\text{V}_2\text{O}_5$  [15,16] appeared in the samples.

Bulk densities of the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.0, 0.1, 0.2, 0.3$ , and  $0.5$ ) ceramics as a function of sintering temperature are shown in Fig. 2. Bulk density of pure  $\text{Bi}_3\text{NbO}_7$  ceramic reached the maximum value when sintering temperature increased to  $930^\circ\text{C}$ . V substitution for Nb effectively decreased sintering temperature of the  $\text{Bi}_3\text{NbO}_7$  ceramic. Bulk densities of the  $\text{Bi}_3(\text{Nb}_{0.9}\text{V}_{0.1})\text{O}_7$  and  $\text{Bi}_3(\text{Nb}_{0.8}\text{V}_{0.2})\text{O}_7$  ceramics got the saturated values when sintering temperature increased to  $840^\circ\text{C}$ . When the content of V substitution increased to 30 and 50 mol%, the optimal sintering temperature increased to  $870^\circ\text{C}$ , which might be caused by appearance of the secondary phase.

SEM and BEI images of as-fired surface of the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics are shown in Fig. 3. All the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ( $x=0.1, 0.2, 0.3, 0.5$ ) ceramics could be well densified when the sintering temperature was around  $840^\circ\text{C}$  and grain size of the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics lay between  $1\sim 3\text{ }\mu\text{m}$  when the V substitution was no higher than 30 mol%. Two kinds of grains were observed obviously in the

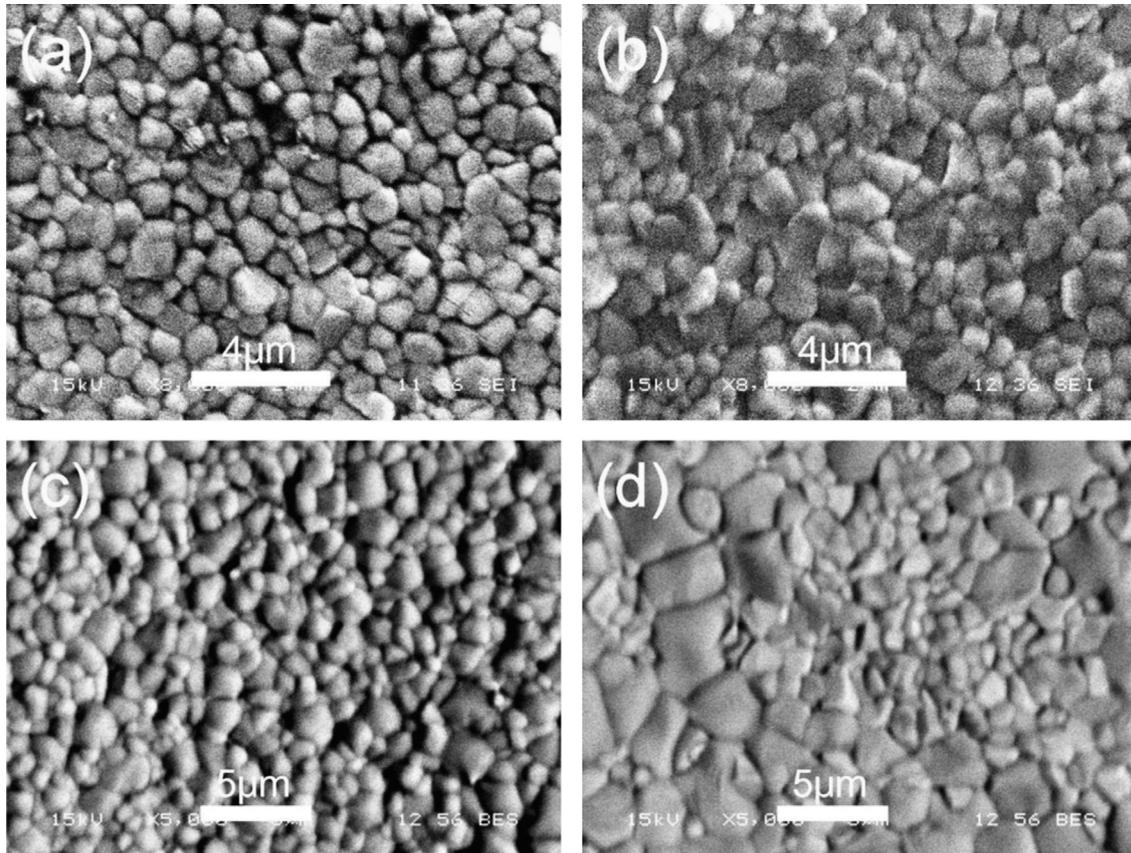


Fig.3. SEM images of as-fired surface of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics sintered at  $840^\circ\text{C}$  for 2 h: (a)  $x=0.1$ , (b)  $x=0.2$ ; Backscatter electron image (BEI) of as-fired surface of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics sintered at  $840^\circ\text{C}$  for 2 h: (c)  $x=0.3$ , (d)  $x=0.5$ .

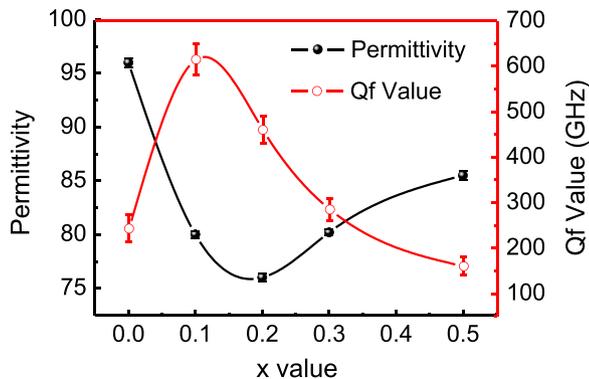


Fig. 4. Microwave permittivity (a) and Qf values (b) of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics.

BEI image of  $\text{Bi}_3(\text{Nb}_{0.5}\text{V}_{0.5})\text{O}_7$  ceramic, as shown in Fig.3 (d). The grains with brighter color and those with darker color and bigger size were corresponding to the Bi-rich phase of  $9\text{Bi}_2\text{O}_3\text{-V}_2\text{O}_5$  and  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  phase, respectively.

Microwave dielectric permittivity and Qf values of the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics are show in Fig. 4. Permittivity and Qf value of pure  $\text{Bi}_3\text{NbO}_7$  ceramic were 96 and 243 GHz respectively, which agreed well with those reported by Valant et al. [10,11]. Permittivity of the  $\text{Bi}_3(\text{Nb}_{0.9}\text{V}_{0.1})\text{O}_7$  ceramic decreased to about 80, and the Qf value increased to 615 GHz.

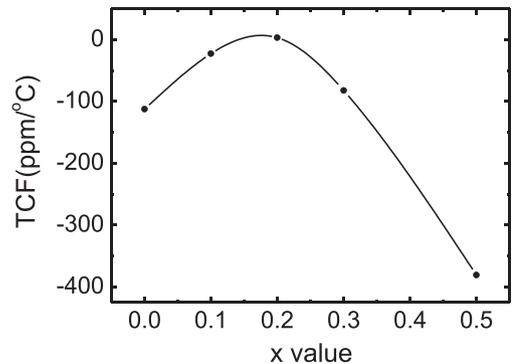


Fig. 5. TCF value of  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics as a function of  $x$  values.

There are two main factors that are responsible for this result. One is the phase transformation from cubic phase to tetragonal phase caused by V substitution (as shown in Fig. 1), and the other is the smaller ionic polarizability of  $\text{V}^{5+}$  ( $2.92 \text{ \AA}^3$ ) than that of  $\text{Nb}^{5+}$  ( $3.97 \text{ \AA}^3$ ) [17]. When the content of V substitution increased to 30 and 50 mol%, dielectric permittivity increased and Qf value decreased seriously, which was mainly caused by the secondary phase of  $9\text{Bi}_2\text{O}_3\text{-V}_2\text{O}_5$ .

TCF value of the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics shifted from  $-112$  to  $3.3 \text{ ppm/}^\circ\text{C}$  when the content of V substitution increased from 0 to 20 mol%, as shown in Fig.5. Then, it shifted to negative value when the content of V substitution

increased further. Temperature stable ( $-30 \text{ ppm}/^\circ\text{C} < \text{TCF} < 30 \text{ ppm}/^\circ\text{C}$ ) low-firing microwave dielectric ceramics were obtained in the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  system when  $x=0.1$  and  $0.2$ . The  $\text{Bi}_3(\text{Nb}_{0.9}\text{V}_{0.1})\text{O}_7$  and  $\text{Bi}_3(\text{Nb}_{0.8}\text{V}_{0.2})\text{O}_7$  ceramics sintered at  $870^\circ\text{C}$  for 2 h possessed high permittivity of 80 and 76, Qf values of 615 and 460 GHz, and TCF values of  $-22$  and  $+3.3 \text{ ppm}/^\circ\text{C}$ , respectively.

#### 4. Conclusions

$\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics were prepared by solid state reaction method. All the ceramics could be well densified when the sintering temperatures were  $840\sim 930^\circ\text{C}$ . The V substitution for Nb in the  $\text{Bi}_3\text{NbO}_7$  ceramic led the composition to crystallize in a tetragonal phase. When the content of V substitution increased to 30 mol% ( $x=0.3$ ), the Bi-rich phase of  $9\text{Bi}_2\text{O}_3\text{-V}_2\text{O}_5$  appeared in the samples. Correspondingly, permittivity of the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  ceramics decreased from 96 to 76 and the TCF value shifted from  $-112$  to  $3.3 \text{ ppm}/^\circ\text{C}$  when the content of V substitution increased from 0 to 20 mol % ( $x=0.2$ ), while the permittivity increased and the TCF value shifted towards negative because of the appearance of secondary phase when the content of V substitution increased further. Temperature stable low-firing microwave dielectric ceramics with high permittivity were obtained in the  $\text{Bi}_3(\text{Nb}_{1-x}\text{V}_x)\text{O}_7$  system when  $x=0.1$  and  $0.2$ . The  $\text{Bi}_3(\text{Nb}_{0.9}\text{V}_{0.1})\text{O}_7$  and  $\text{Bi}_3(\text{Nb}_{0.8}\text{V}_{0.2})\text{O}_7$  ceramics sintered at  $870^\circ\text{C}$  for 2 h possessed high permittivity of 80 and 76, Qf values of 615 and 460 GHz, and TCF values of  $-22$  and  $+3.3 \text{ ppm}/^\circ\text{C}$ , respectively.

#### Acknowledgments

This work was supported by NSFC project of China (51202182 and 51202178), the Natural Science Foundation of Shaanxi Province (2014JQ6200).

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