



Fabrication and characterization of porous titanium-based PbO₂ electrode through the pulse electrodeposition method: Deposition condition optimization by orthogonal experiment[☆]

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HIGHLIGHTS

- Novel PbO₂ anodes were fabricated through pulse electrodeposition.
- The effects of pulse electrodeposition parameters on PbO₂ characters were evaluated.
- An optimized pulsed electrodeposition parameter is presented.
- The brief mechanism of pulse electrodeposition is uncovered.

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ABSTRACT

Porous titanium-based PbO₂ electrodes were successfully fabricated by pulse electrodeposition method. The primary pulse electrodeposition parameters, including pulse frequency (f), duty ratio (γ), average current density (J_a) and electrodeposition time (t) were considered in this study. An orthogonal experiment was designed based on those four factors and in three levels. SEM images and XRD results suggest that the surface morphology and structure of PbO₂ electrodes could be easily changed by varying pulse electrodeposition parameters. Orthogonal analysis reveals that the increase of f and J_a could decrease the average grain size of PbO₂ electrodes, which is conducive to create more active sites and promote the generation of hydroxide radicals. The electrochemical degradation of Azophloxine was carried out to evaluate the electrochemical oxidation performance of pulse electrodeposited electrodes. The results indicate that the influences of four factors can be ranked as follow: $J_a > \gamma \approx t > f$. The higher f , larger J_a and longer t could facilitate the optimization of the integrated electrochemical degradation performance of prepared PbO₂ electrode. The accelerated life time is dominated by J_a and t , coincident with the average weight increase of β -PbO₂ layer. The optimal parameters of pulse electrodeposition turn out to be: $f = 50$ Hz, $\gamma = 30\%$, $J_a = 25$ mA cm⁻², $t = 60$ min. Together, the consequences of the experiments give assistance to uncover and roughly conclude the mechanism of pulse electrodeposition.

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1. Introduction

Electrochemical advanced oxidation is an attractive and promising technique for organic pollutants removal because of its

environmental friendliness, easy accessibility and mineralization effectiveness (Nidheesh et al., 2018; Zhang et al., 2019a). In electrochemical advanced oxidation process, strong oxidizing agents are generated in the vicinity of anode to degrade the organics into carbon dioxide, water and inorganic ions (Miklos et al., 2018; Yang et al., 2019; Yao et al., 2019a).

Anode material plays a crucial role during electrochemical oxidation process, directly influencing the efficiency of the degradation and mineralization for targeted contaminants (Xu et al., 2019c; Yao et al., 2019b; Zahorulko et al., 2019). Therefore, a series of anode materials have been investigated in previous works,

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such as SnO₂ (Bi et al., 2019; Chen et al., 2019; Zhang et al., 2019c), boron-doped diamond (BDD) (Mei et al., 2019; Cornejo et al., 2020; Suzuki et al., 2020), IrO₂ (Hu et al., 2014; Baddouh et al., 2019; Sun et al., 2020), PbO₂ (Wang et al., 2019; Zhou et al., 2020), Ti₄O₇ electrode (Lin et al., 2018; Wang et al., 2020), and compound electrodes (Yuan et al., 2019; Shao et al., 2020). Pure SnO₂ is an n-type semiconductor with low conductivity at room temperature, which needs to be improved by various elements doping (Rao and Venkatarangaiah, 2014). BDD electrode shows an extremely wide potential window, but is restricted in the large-scale application due to its high cost of synthesis, while IrO₂ electrode is favorable to oxygen evolution side reaction because of its low oxygen evolution potential (OEP) (Panizza and Cerisola, 2009). Ti₄O₇, a Magnéli phase titanium sub-oxide, is proposed as a promising anode material for its great conductivity and chemical stability, however the passivation during anodic polarization is still a problem to be further addressed (Chaplin, 2014).

Among them, PbO₂ electrode has been widely applied in electrochemical oxidation because of its prominent electro-catalytic performance, mineralization effect and low cost (Dargahi et al., 2019; Qian et al., 2019; Tammam and Hassan, 2019). However, there are still some drawbacks of PbO₂ electrode requiring improvement, such as Pb leakage, low hydroxide radical utilization and OEP. In order to solve those problems, many efforts have been made by different approaches, including substrate and inner layer modification (SnO₂–Sb inner layer (Yu et al., 2018; Xu et al., 2019b), TiO₂ nanotubes inner layer (Wang et al., 2018; Wu et al., 2019), carbon nanotubes inner layer (Xu et al., 2019a), stainless steel substrate (Elaiassaoui et al., 2019)), elements doping (Xia and Dai, 2018; Bian et al., 2019; Chen et al., 2020), particle incorporation (Duan et al., 2019; Tang et al., 2020) and surfactant modification (Duan et al., 2018; Velichenko et al., 2020).

Moreover, the change of PbO₂ fabrication technique also could lead significant variation of electrode morphology and property (Boukhchina et al., 2019). Recently, pulse electrodeposition method was introduced to PbO₂ electrodes preparation in order to increase surface active site and improve the electrocatalytic capability of PbO₂ electrode (Hakimi et al., 2019). He et al. (2018) investigated the effect of different duty cycles in pulse reverse current (PRC) electrodeposition, and pointed out that crystal structure and morphology of PbO₂ observably altered after PRC deposition, which rise the content of β phase and create a rough surface of morphologic feature. Yao et al. (2017) explored the effects of peak current density on the characteristics of PbO₂–CeO₂ nanocomposite electrodes, of which the results showed that the increase of peak current density could make the morphology finer and more compact, as well as reduce the crystal size. Various parameters of pulse electrodeposition have been severally investigated in detail, whereas, the parameters are not complete independent with each other. The relations among those factors show as follows:

$$f = \frac{1}{T_p + T_v} \quad (1)$$

$$\gamma = \frac{T_p}{T_p + T_v} \quad (2)$$

$$J_a = (J_p + J_v)\gamma \quad (3)$$

where f is the frequency, T_p is the peak value time, T_v is the valley value time, γ is the duty ratio, J_a is the average current density, J_p is the peak value current density and J_v is the valley value current density. Therefore, it is necessary to study the comprehensive effects of different pulse electrodeposition parameters on the

characteristics of PbO₂ electrode.

In this study, porous titanium based PbO₂ electrodes were fabricated through pulse electrodeposition method. Porous titanium, a common anti-corrosion filter element, was chosen as the substrate material of PbO₂ electrode, because the porous structure could improve the specific surface area of electrodes. Orthogonal experiment was designed to explore the optimum pulse electrodeposition parameters and systematically analyze the influences of each parameter on the electrode properties. The most important operating parameters of pulse electrodeposition, including pulse frequency (f), duty ratio (γ), average current density (J_a) and the time (t) of electrodeposition, were selected as four factors, along with three levels under every factor. L9 orthogonal array were chosen for this work. The normal PbO₂ electrode fabricated by direct current electrodeposition was assigned as the control group. The prepared PbO₂ electrodes were characterized by scanning electron microscopy (SEM), X-ray diffraction (XRD), cyclic voltammetry (CV) sweep and electrochemical impedance spectroscopy (EIS). The hydroxide radical productivities of prepared electrodes were also tested in order to estimate the electrochemical oxidation capabilities. Following from that, the prepared electrodes were used as the anodes for the electrochemical degradation of Azo-phloxine (AR1) for purpose of the comprehensive electrochemical degradation performance evaluation. Ultimately, the electrode stabilities were characterized by the accelerated lifetime and the elements leakage tests. Furthermore, the pulse electrodeposition mechanisms are briefly summarized based on the results.

2. Materials and methods

2.1. Materials

All chemicals used in this work purchased from Sinopharm Chemical Reagent Co., Ltd, were of analytical grade without further purification. The aqueous solutions were deionized water (18 MΩ cm⁻¹, EPED-S2-D, Nanjing, China). Unless otherwise specified, all the experiments were done at room temperature.

2.2. Preparation of substrates and fabrication of inner layer

Porous titanium plates (Filter Fineness = 80 μm, Baoji Yinggao metal material Ltd., China) with a dimension of 2 cm × 5 cm × 1 mm were used as the electrode substrate. The pretreatment of porous Ti plate and introduction of intermediate Sb–SnO₂ layer and α-PbO₂ layer were the same as our previous work (Li et al., 2016a, 2016b, 2017; Wu et al., 2019).

2.3. Electrodeposition of surface β-PbO₂ layer

The surface β-PbO₂ layer was coated on the Ti/Sb–SnO₂/α-PbO₂ electrode via anodic deposition process. The plating bath was composed of 0.5 M Pb(NO₃)₂, 0.2 M Cu(NO₃)₂ and 0.01 M NaF. The solution pH value was adjusted to 2.0 with the concentrated HNO₃.

2.3.1. Direct current electrodeposition

Setting the current density as 20 mA cm⁻², the temperature was controlled at 65 °C for 120 min for the direct current deposition processing. The same titanium mesh served as the counter cathode. And we marked the fabricated electrodes as PbO₂(DC).

2.3.2. Design of orthogonal experiment

The pulse electrodeposition processes were conducted at 65 °C, the valley value current density was maintained at 0 mA cm⁻², so the peak value current density could be determined by the γ and the J_a . The titanium mesh with the same dimension served as the

counter cathode.

The primary electroplating parameters of f , γ , J_a and t were considered in this study. This experiment was designated as $L_9(3^4)$ orthogonal array, which chose four plating parameters and three levels. The factors and levels of the orthogonal experiment are listed in Table SM-1, and the L_9 orthogonal arrays are presented in Table SM-2.

As shown in Fig. 1, the fabricated electrodes were marked as $PbO_2(P1\sim9)$ respectively, in accordance with the experiment number in Table SM-2. Furthermore, all test results from pulse electrodeposition electrodes ($PbO_2(P1\sim9)$) in this work would be normalized with that from constant current electrodeposition ($PbO_2(DC)$) as the base, before doing orthogonal analysis. The data were normalized as follow:

$$X_i' = \frac{X_i}{X_{DC}} \quad (4)$$

where X_i' is the normalization coefficient of X_i , X_i is the test result of $PbO_2(P_i)$, i is the experiment number in Table SM-2, X_{DC} is the test result of $PbO_2(DC)$.

2.4. Characterization

SEM (Techcomp, SU3500) was employed for characterizing the surface morphology of samples. XRD (SHIMADZU, XRD-6100) analyses were performed using a diffractometer with Cu-K α radiation.

A three-electrode cell was adopted to perform all electrochemical measurements at room temperature. The prepared electrodes act as the working electrodes, respectively. Ag/AgCl/saturated KCl electrode was selected as the reference electrode and platinum sheet as counter electrode. CV sweep was conducted in 0.5 M Na_2SO_4 solution at 10 $mV s^{-1}$ in the range of 0–2.5 V. EIS measurement was conducted in 0.5 M Na_2SO_4 solution with a measurement potential of 0 V (vs Ag/AgCl), of which the frequencies swept from 10^5 Hz to 10^{-2} Hz with a sine wave in 5 mV amplitude.

The electrochemical oxidation capacity was assessed by comparison for the yields of hydroxyl radical ($\cdot OH$) from different electrodes. The HPLC (Sykam, S500) with dimethyl sulfoxide (DMSO) trapping was used to test the $\cdot OH$ concentration after 1-h electrolysis (Xu et al., 2018).

The accelerated lifetime tests were conducted at constant

current density of 500 $mA cm^{-2}$ in 3 M H_2SO_4 for electrode stability evaluation ($35 \pm 2 \text{ }^\circ C$). The titanium mesh act as the counter electrode. The prepared electrode was employed as the working electrode, which was deemed as deactivation when the cell voltage came to 10 V.

2.5. Electrochemical oxidation test

The electrochemical oxidation for Azophloxine (AR1, $C_{18}H_{13}N_3NaO_8S_2$, CAS no. 3734-67-6) were implemented in 250 mL synthesized wastewater containing 200 $mg L^{-1}$ AR1 with 10 $g L^{-1}$ Na_2SO_4 as the supportive electrolyte. The electrode prepared was used as the anode and titanium mesh as the cathode. The distance between anode and cathode was maintained at 1.0 cm. The electrochemical oxidation process was carried out in constant current of 30 $mA cm^{-2}$ (the working electrode area of 10 cm^2) with a magnetic stirrer for 120 min. The samples were monitored and analyzed every 30 min. UV–Vis absorption (UV2600A, Unico, Shanghai, China) was employed to test the concentration of AR1 at the characteristic wavelength of 506 nm (Zhang et al., 2019b; Lei et al., 2020). COD was measured by a commercial COD detector (Multi Direct, Lovibond), and TOC was assayed by ET1020A TOC analyzer.

The % of COD removal (R_{COD}) and % of TOC removal (R_{TOC}) of AR1 in electrochemical degradations were calculated as follows:

$$R_{COD} = \frac{COD_0 - COD_t}{COD_0} \times 100\% \quad (5)$$

$$R_{TOC} = \frac{TOC_0 - TOC_t}{TOC_0} \times 100\% \quad (6)$$

where COD_0 and COD_t are the chemical oxygen demands, TOC_0 and TOC_t are the total organic carbon at the initial and end, respectively.

In addition, the electrochemical oxidation effect of the PbO_2 electrodes on AR1 was assessed through average current efficiency (ACE) and energy consumption per unit COD mass (EC_{COD} , $kWh gCOD^{-1}$), which were calculated as follows:

$$ACE = \frac{COD_0 - COD_t}{8It} FV \times 100\% \quad (7)$$

$$EC_{COD} = \frac{Ult}{(COD_0 - COD_t)V} \quad (8)$$

where F is the Faraday constant ($96,487 C mol^{-1}$), V is the volume of the electrolyte (L), I is the current (A), t is the time (min) and U is the cell voltage (V).

Additionally, degradation index (DI) was established in order to compare the electrochemical oxidation performance of pulse electrodeposition electrodes. The DI was calculated as follow:

$$DI = R'_{COD} + R'_{TOC} + GCE' - EC'_{COD} \quad (9)$$

where R_{COD}' , R_{TOC}' , ACE' and EC_{COD}' are the normalization coefficients of R_{COD} , R_{TOC} , ACE and EC_{COD} , respectively.

3. Results and discussion

3.1. Surface morphology and structure

As shown in Fig. 2, the surface morphology of prepared electrodes indicates significant differences of structure and particle size among those. Following the raising of t and J_a , a significant increase in PbO_2 particle size was recorded. In Fig. 2c, d, 2e, 2f and 2h, there

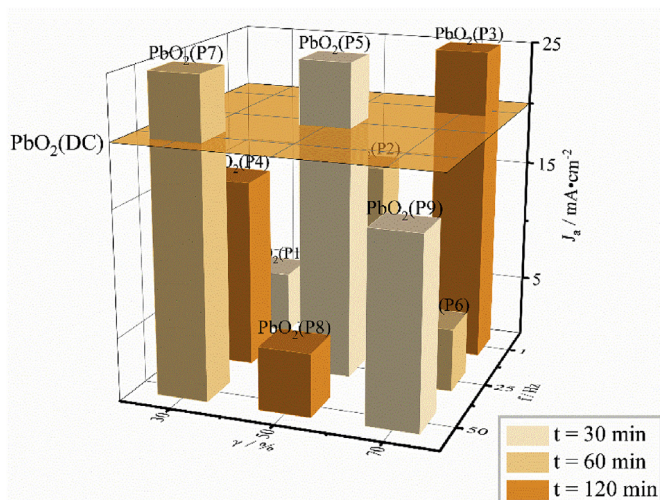


Fig. 1. Orthogonal experiment design of pulse electrodeposition.

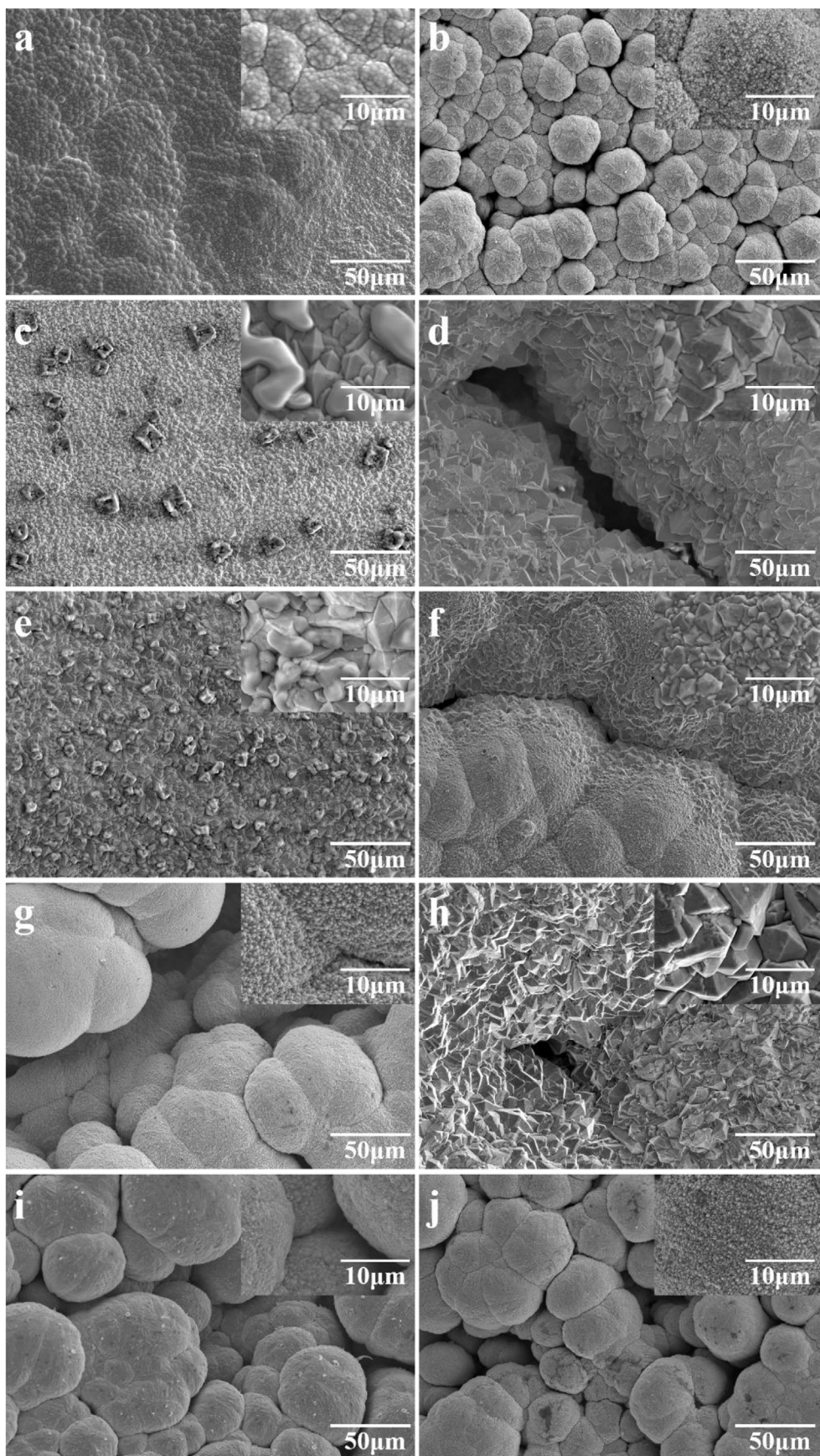


Fig. 2. SEM images of prepared electrodes, (a) $\text{PbO}_2(\text{DC})$, (b) $\text{PbO}_2(\text{P1})$, (c) $\text{PbO}_2(\text{P2})$, (d) $\text{PbO}_2(\text{P3})$, (e) $\text{PbO}_2(\text{P4})$, (f) $\text{PbO}_2(\text{P5})$, (g) $\text{PbO}_2(\text{P6})$, (h) $\text{PbO}_2(\text{P7})$, (i) $\text{PbO}_2(\text{P8})$, (j) $\text{PbO}_2(\text{P9})$.

are typical pyramidal shape, while some indefinite shape could be observed in Fig. 2c, e and 2f, coincident with findings in other reports (Elaiassaoui et al., 2019; Ansari and Nematollahi, 2020). Interestingly, three-dimensional cauliflower shape which could be fabricated by Ce doping (Lyu et al., 2019), was frequently observed in the electrodes made by pulse electrodeposition with high f and γ . The PbO_2 electrodes deposited in methanesulfonate bath showed the same fine and compact surface morphology without three-dimensional structure (He et al., 2019). As shown in Fig. SM-1, porous titanium was chosen as the substrate of PbO_2 electrodes to expand the surface area. The surface morphology and porous structure were improved by acid etch and inner layer coating. It is apparent from Fig. 2 that surface PbO_2 layer shows porous morphology in every prepared electrode except $\text{PbO}_2(\text{DC})$, $\text{PbO}_2(\text{P2})$ and $\text{PbO}_2(\text{P4})$, which means that porous PbO_2 layer could be formed more easily under high frequency pulse. Moreover, the uniform and compact surface could be obtained on the electrodes deposited in high frequency pulse, which may be because the pulse electrodeposition has ability to alleviate the concentration polarization during the fabrication process (shown as Fig. 4).

Fig. 3 displays XRD patterns of the prepared electrodes by the constant current electrodeposition and the pulse electrodeposition. What stands out in Fig. 3 is the presences of α - PbO_2 in pulse deposition PbO_2 electrodes, compared with $\text{PbO}_2(\text{DC})$. The diffraction peaks located at 25.39° , 31.94° , 36.16° and 49.13° correspond to the lattice planes (110), (101), (200) and (211) of β - PbO_2 (75-2420)

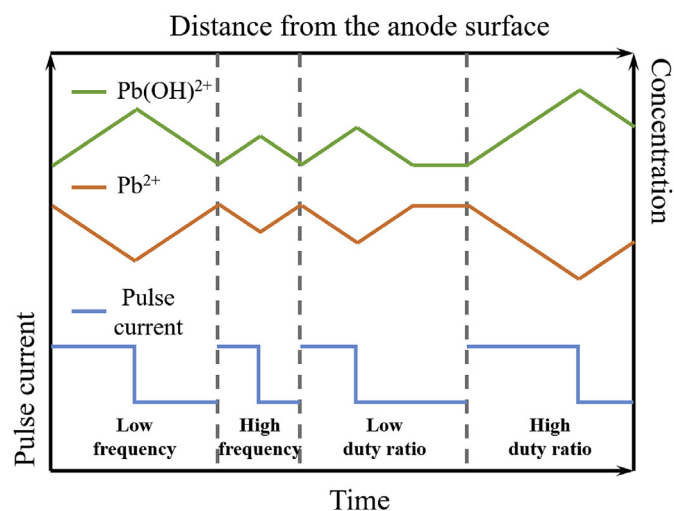


Fig. 4. Concentration variations of Pb^{2+} and $\text{Pb}(\text{OH})^{2+}$ in the electrolyte during pulse electrodeposition processes with different parameters.

respectively. The other characteristic peaks at 28.40° , 32.63° , 36.02° , 38.40° , 39.81° , 44.92° , 49.32° and 52.35° correspond to the lattice planes (111), (002), (200), (121), (112), (022), (202) and (131) of α - PbO_2 (75-2414) respectively. It may prove that pulse

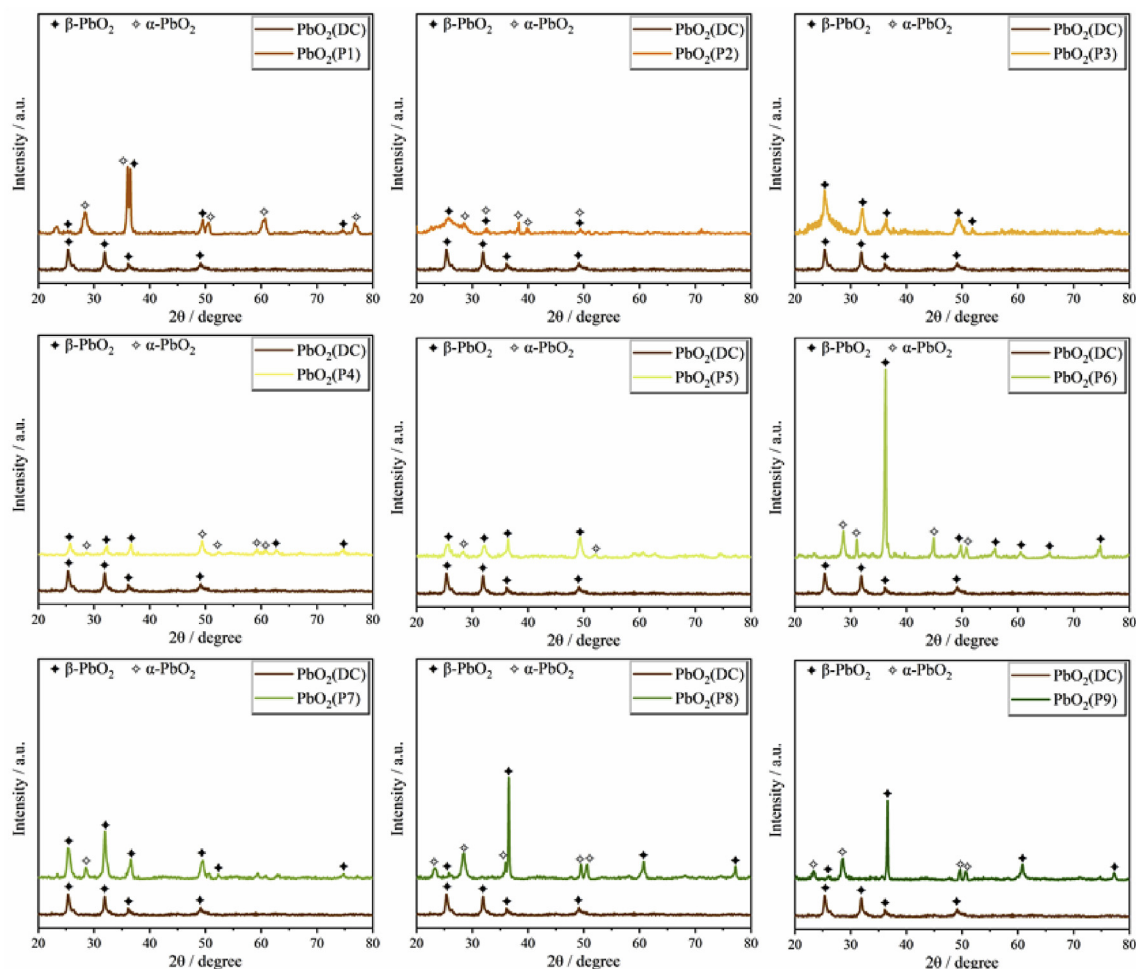


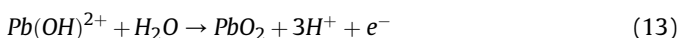
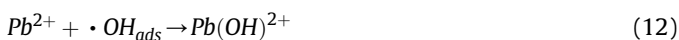
Fig. 3. XRD patterns of prepared electrodes.

electrodeposition can change the crystallization process of PbO₂. Comparing the XRD patterns in Fig. 3, the electrodes (PbO₂(3), PbO₂(5), PbO₂(7)) belonging to high J_a ($J_a = 25 \text{ mA cm}^{-2}$) group mainly show diffraction peaks of β -PbO₂, which may indicate that high J_a is beneficial to form pure β -PbO₂. Moreover, it is clear that the diffraction patterns of PbO₂(P7), PbO₂(P8) and PbO₂(P9) are sharp and strong, demonstrating that well-crystallized PbO₂ could be obtained by pulse electrodeposition with high frequency.

The average grain sizes of surface PbO₂ crystal are presented in Table 1, which were calculated by Debye–Scherrer equation:

$$D = \frac{k\lambda}{\beta \cos \theta} \quad (10)$$

where D is the crystallite size, λ is the X-ray wavelength, β is the full width at half maximum of the strongest diffraction peak and θ is the diffraction angle. After normalization and orthogonal analysis of grain size data (shown in Table SM-3), it could be concluded that J_a and f are the primary influence factors on grain size. The PbO₂ nucleation mechanism can be illustrated as Eq. 11–13 (Sun et al., 2019). When current is applied at the anode, a small quantity of adsorbed ·OH are initially generated on the anode surface (Eq. (11)). The aqueous Pb²⁺ would diffuse toward the anode surface via convective diffusion and then react with ·OH with the formation of the soluble intermediates (Pb(OH)²⁺) by Eq. (12), eventually, the Pb(OH)²⁺ is electrochemically oxidized to PbO₂ (Eq. (13)).



There was a significant negative correlation between J_a and average grain size. In other word, increase of J_a is helpful to minify PbO₂ crystal, coincident with traditional PbO₂ electrodeposition mechanism (Velichenko et al., 2009; Sirés et al., 2010). Nonetheless, the analysis result revealed that PbO₂ average grain size increased sharply when f reached 50 Hz, attributed to the poly-crystal aggregate occurring in high frequency pulse.

Combine previous studies about cathodic pulse electrodeposition mechanism (Ye et al., 2018, 2020), Fig. 4 illustrates the concentration variations of Pb²⁺ and Pb(OH)²⁺ in the electrolyte during pulse electrodeposition processes with different parameters. Crystal size is determined together by nucleation and growth process. On the one hand, high J_a brings more nucleation, which helps to form small crystal. On the other, high f diminishes concentration polarization effectively, which could promote high valence state metal ion migration then restrain nucleation process, therefore growth process rules in electrodeposition and crystal size increases. The increase of γ could however impair the influence

resulted from high f , driving the process to present more similarly to direct electrodeposition. Interestingly, the average grain size of PbO₂(P7) was smaller than that of other electrodes made by high frequency pulse. It means that when J_a reached 25 mA cm^{-2} , nucleation was strong enough to re-dominate the electrodeposition process, resulting in the small size of PbO₂ crystal. To sum up, there is no change of electrodeposition mechanism in essence after introducing pulse current supply mode, whereas it is notably that, through regulating the pulse parameters, the crystal nucleation and growth process could be balanced so as to optimize the structure and morphology of fabricated PbO₂ electrode.

3.2. Electrochemical test

3.2.1. CV

Fig. SM-2 shows the CV curves of prepared PbO₂ electrodes. The anodic peaks appeared on approximately 1.25 V, because PbO₂ is a nonstoichiometric compound and the ratio of oxygen to lead was lower than the stoichiometric ratio, so that some low-valent lead compounds in the active layer were oxidized to that of high-valent. The upsurge of anodic current can be observed at 1.8–2.0 V for all electrodes, which could be attributed to oxygen evolution reaction. It could be seen that the current responses are enhanced prominently by pulse electrodeposition, which indicates that pulse electrodeposition favors charge exchange. PbO₂(P7) shows the highest current response, which means the superior conductivity of PbO₂(P7). Table 1 presents the OEP and voltammetric charge which were calculated from CV test. The highest (1.94 V) and lowest (1.84 V) OEP were obtained at PbO₂(P5) and PbO₂(DC) respectively, similar to other porous PbO₂ electrode (Liu et al., 2017). It therefore could be interpreted that partial α -PbO₂ presence would not make distinct difference to the OEP of PbO₂ electrode. The electrochemical activity of an electrode can be evaluated through the voltammetric charge (q^*), related to the number of active sites. Higher value of q^* represents greater electrode activity for the identical electrode material. The q^* was acquired via integrating the cycle voltammetric curves over the entire potential range from 0 to 2.5 V (Xu et al., 2016). The results of calculation and orthogonal analysis of voltammetric charge (Fig. 5a and Table SM-4) shows that f was the dominating influence factor which positively correlated to voltammetric charge significantly. It could be explained by the results of SEM and XRD that high frequency pulse avails to form well crystallized, finer and porous surface PbO₂ layer, which is favorable to build more active sites and promote electrochemical oxidation ability (Wang et al., 2017; Weng and Yu, 2019).

3.2.2. EIS

EIS test results and equivalent circuit are shown in Fig. 5b and Table SM-5. The equivalent circuit and the simulation of parameters of EIS spectra were evaluated by ZSimDemo software, which indicated that the test data of all prepared electrodes well fitted in the

Table 1
Various characterization parameters of prepared electrodes.

Sample	Crystal size (nm)	OEP (V)	Voltammetric charge (C cm ⁻²)	Accelerated lifetime (h)
PbO ₂ (DC)	17.7	1.84	1.33	152
PbO ₂ (P1)	30.1	1.90	1.58	138
PbO ₂ (P2)	13.6	1.92	0.87	192
PbO ₂ (P3)	14.4	1.94	0.84	268
PbO ₂ (P4)	15.3	1.91	0.7	272
PbO ₂ (P5)	9.5	1.94	1.44	173
PbO ₂ (P6)	27.1	1.89	1.58	137
PbO ₂ (P7)	16.9	1.93	1.48	212
PbO ₂ (P8)	41.2	1.89	1.8	158
PbO ₂ (P9)	40.2	1.88	1.87	146

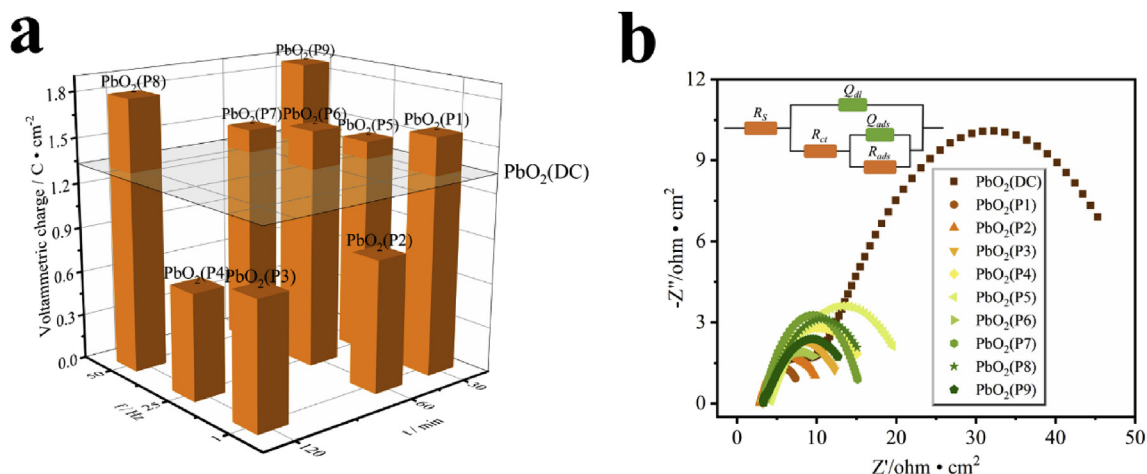


Fig. 5. (a) Voltammetric charge of prepared PbO₂ electrodes, (b) Nyquist diagrams and equivalent circuit of prepared PbO₂ electrodes.

equivalent circuit in Fig. 6. R_s represents the uncompensated solution resistance; CPE_1 the double layer capacitance (Q_{dl}); R_{ct} the charge transfer resistance; CPE_2 the adsorption pseudo capacitance of the reaction intermediates (Q_{ads}); R_{ads} the resistance imposed by the reaction intermediates adsorbed at the electrode surface (Yang et al., 2012). As can be seen from the figure above, the arc diameters of electrodes fabricated by pulse electrodeposition is significantly smaller than that of PbO₂(DC), which further supports the conclusion from CV that pulse electrodeposition is conducive to charge exchange.

3.3. Productivity of hydroxide radical

OH are generated from the oxidation of water, as shown in Eq. (14), which is the core of electrocatalytic reaction (Lei et al., 2020; Yijing Xia, 2020):



OH were measured by an indirect method with dimethyl sulfoxide (DMSO) as the capture agent. OH reacts with DMSO to generate formaldehyde, then with 2, 4-dinitrophenylhydrazine (DNPH) to generate corresponding hydrazone (HCHO-DNPH), and is finally detected by HPLC. The content of OH can be calculated by the content of formaldehyde, which could be determined by HPLC. Fig. SM-3 compares the OH productivities of pulse electrodeposition PbO₂ electrodes and PbO₂(DC). The OH concentrations of the electrodes fabricated by pulse electrodeposition were all higher than that of PbO₂(DC). Combining with the results of XRD, a possible explanation is that the decrease of crystal size and porous morphology could create more active sites to accelerate OH production.

The result of normalization and orthogonal analysis (listed as Table SM-6) reveals the positive correlation between hydroxide radical productivity and t . And γ , which directly affects real deposition time, also facilitate hydroxide productivity. Those two correlations suggest that the real electrodeposition time should not be too short otherwise hydroxide radical productivity will be impaired. However, the primary factor that affects hydroxide radical productivity is f . In addition, the productivity of OH would be raised prominently by high frequency pulse, which is coincident with the orthogonal analysis result of voltammetric charge.

3.4. Electrochemical oxidation performance

Fig. 6 and Fig. SM-4 display the results of AR1 degradation in

order to identify the electrode with the best electrochemical oxidation performance. Fig. SM-4 shows that simulated AR1 wastewater were decolorized after 120-min electrochemical oxidation. R_{COD} data of pulse electrodeposition electrodes were compared with that of PbO₂(DC) in Fig. 6a. As shown in Fig. 6b, the $\ln(C_t/C_0)$ of COD test results were well fitted in pseudo-first-order kinetic. Except PbO₂(P1) and PbO₂(P6), R_{COD} of all electrodes fabricated by pulse electrodeposition were higher than that of PbO₂(DC). The electrodes belonging to high frequency group ($f = 50$ Hz) presented better COD removal capacity than others. In addition, PbO₂(P7) attained the highest R_{COD} (82.3%) which was 1.4 times higher than PbO₂(DC), as well as the highest k value which is 1.6 times as high as PbO₂(DC). R_{TOC} is an important index to evaluate the mineralization capacity of electrodes. From Fig. 6e and Table SM-7, it could be seen that PbO₂(P3), PbO₂(P5) and PbO₂(P7) electrodeposited in high J_a pulse performed better mineralization effect. According to XRD results, a possible explanation is that β -PbO₂ proportion, which can be increased by raising J_a during pulse electrodeposition, is important to enhance the mineralization ability of PbO₂ electrode. For the consideration of energy conservation, ACE and EC_{COD} are necessary to assess the electrochemical oxidation performance of electrode materials. Fig. 6c and d compare ACE and EC_{COD} between prepared electrodes respectively, and the data of those could be found in Table SM-7. PbO₂(P2) showed the highest ACE (12% improvement over PbO₂(DC)) and the lowest EC_{COD} (24% reduction under PbO₂(DC)), but the R_{COD} and R_{TOC} of PbO₂(P2) were insufficient than satisfactory target. Hence, DI (the computing method was showed in Eq. (9)) was introduced to evaluate and compare the electrochemical oxidation performance of prepared electrodes comprehensively and expediently. Fig. 6f exhibits the comparison of DI , where most pulse electrodeposition electrodes performed greater electrochemical degradation capacity of AR1. Meanwhile, PbO₂(P7) showed the best degradation capacity, which was 41% higher than PbO₂(DC) in degradation, and further exhibited the more favorable performance than PbO₂(DC) in all aspects.

The orthogonal analysis results of DI (shown as Table SM-8) suggest that the influences of four factors can be ranked as follow: $J_a > \gamma \approx t > f$. The large J_a , long t , moderate γ and high f are conducive to optimize the whole electrochemical degradation performance of PbO₂ electrode. Large J_a and long t are helpful to promote β -PbO₂ layer attachment. Besides, the coordination of moderate γ and high f is in favor of properly porous and compact surface structure. All of them improve the COD and TOC removal ability of PbO₂ electrode together, and the current efficiency is also optimized.

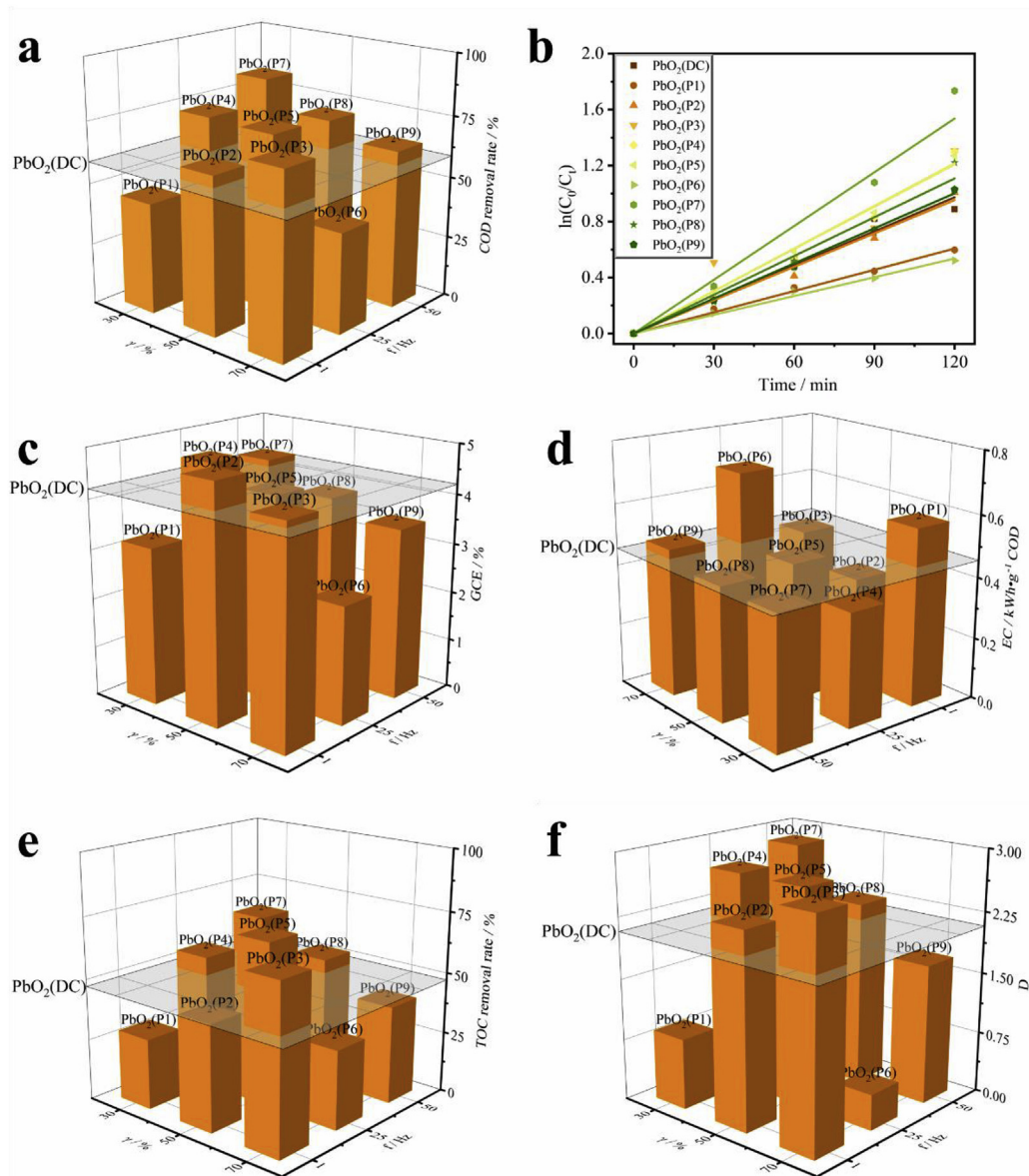


Fig. 6. AR1 degradation results of prepared electrodes.

3.5. Electrode stability

According to the accelerated lifetime test results shown in Fig. SM-5 and Table 1, pulse electrodeposited PbO₂ electrodes exhibited greater stability than that of PbO₂(DC). The accelerated lifetime of PbO₂(P4) reached up to 272 h, which was the longest and 1.79 times as long as that of PbO₂(DC) (152 h). Comparing with previous studies about porous PbO₂ electrode (Xu et al., 2019a), the accelerated lifetime of PbO₂(P4) was much longer. The lifetime increase of pulse electrodeposited PbO₂ could be explained by that pulse electrodeposition makes the PbO₂ surface more compact, preventing the penetration of electrolyte, thus conducive to improve the stability of PbO₂ electrode (He et al., 2019; Zhang et al., 2020).

The orthogonal analysis results are displayed in Table SM-9. The t and J_a were main influence factors on the accelerated lifetime of PbO₂ electrode. The accelerated lifetime positively correlates to those two parameters which are highly correlated with the average

weight increase of PbO₂ layer (Table SM-10). It means that average weight increase of PbO₂ layer is crucial for extending service life of PbO₂ electrode.

Fig. SM-6 shows the Pb²⁺ leakage of prepared electrodes after 2 h electrolysis in 0.1 M Na₂SO₄ solution. All electrodes fabricated by pulse electrodeposition exhibited better safety than that of PbO₂(DC) except PbO₂(P3) and PbO₂(P4). It is because fine grain size and compact surface could promote the anti-corrosion ability of PbO₂ electrode. According to the average weight increase (Fig. SM-7), the high Pb²⁺ leakage of PbO₂(P3) and PbO₂(P4) could be ascribed to the high weight augment.

4. Conclusions

PbO₂ electrodes with different morphology and characters were successfully fabricated by pulse electrodeposition. SEM and XRD results indicated that pulse electrodeposition was conducive to fabricate uniform and compact structure. Electrochemical test

results suggested that pulse electrodeposition facilitated charge exchange. Hydroxide radical productivity test results revealed that pulse electrodeposition was helpful to create more active sites which highly correlates with hydroxide radical productivity. $\text{PbO}_2(\text{P7})$ exhibited the best electrochemical oxidation ability. The COD and R_{TOC} of $\text{PbO}_2(\text{P7})$ was 82.3% and 64.0% respectively. Accelerated lifetime and Pb^{2+} leakage test results showed that pulse electrodeposition could evidently promote the stability of PbO_2 electrode. Orthogonal analysis indicated that f positively correlated with voltammetry charge and hydroxide radical productivity. Whereas, J_a was the major influence factor on comprehensive electrochemical degradation performance of PbO_2 electrode. The influences of four factors can be ranked as follow: $J_a > \gamma \approx t > f$. In addition, the J_a and t presents highly positive correlation with electrode stability. Considering the degradation performance and electrode stability, the optimal parameters of pulse electrodeposition were: $f = 50\text{Hz}$, $\gamma = 30\%$, $J_a = 25 \text{ mA cm}^{-2}$, $t = 60 \text{ min}$.

Together, based on aforesaid results, the pulse electrodeposition mechanism could be revealed and roughly concluded as follows: (i) Pulse current supply mode will not essentially change the basic PbO_2 electrodeposition mechanism. (ii) Pulse frequency(f) and duty ratio(γ) influence PbO_2 structure and morphology by adjusting the concentration polarization during electrodeposition process. (iii) Average current density(J_a) and deposition time(t) together decide total content of PbO_2 attached through electrodeposition. (iv) The combination of high f , low γ , large J_a and enough t could fabricate uniform and compact PbO_2 layer with fine crystal size, which shows great degradation performance and stability.

CRediT authorship contribution statement

Guo Hua: Conceptualization, Methodology, Investigation, Writing - original draft. **Xu Zhicheng:** Writing - review & editing. **Qiao Dan:** Methodology, Investigation. **Wan Dan:** Methodology, Investigation. **Xu Hao:** Conceptualization, Methodology, Writing - review & editing. **Yan Wei:** Supervision, Writing - review & editing. **Jin Xiaoliang:** Supervision, Writing - review & editing.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

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Appendix A. Supplementary data

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