



第三章 流体力学的几个重要定理

3.1 开尔文定理

3.2 伯努利方程

3.3 非惯性系中的伯努利方程

3.4 涡量动力学方程



3.1 开尔文定理

开尔文定理



对于正压、质量力单值有势的理想流体流动、沿任意封闭的物质周线上的速度环量和通过任一物质面的涡通量在运动过程中守恒

证明：设由确定的流体质点组成的封闭物质线 $C(t)$ ，其位置和形状随流动而变化

$$\begin{aligned} \longrightarrow \quad \frac{D\Gamma}{Dt} &= \frac{D}{Dt} \oint_{C(t)} \vec{u} \cdot d\vec{r} = \oint_{C(t)} \left[\frac{D\vec{u}}{Dt} \cdot d\vec{r} + \vec{u} \cdot \frac{D(d\vec{r})}{Dt} \right] \\ &= \oint_{C(t)} \left[\frac{D\vec{u}}{Dt} \cdot d\vec{r} + \vec{u} \cdot d\vec{u} \right] \end{aligned}$$



开尔文定理2

速度矢量为单值函数

$$\Rightarrow \oint_{C(t)} \vec{u} \cdot d\vec{u} = \oint_{C(t)} d\left(\frac{u^2}{2}\right) = 0$$

$$\Rightarrow \frac{D\Gamma}{Dt} = \oint_{C(t)} \left[\frac{D\vec{u}}{Dt} \cdot d\vec{r} + \vec{u} \cdot d\vec{u} \right] = \oint_{C(t)} \frac{D\vec{u}}{Dt} \cdot d\vec{r} = \oint_{C(t)} \frac{Du_i}{Dt} \cdot dx_i$$

加速度环量

- 沿一条由流体质点组成的物质周线的速度环量的随体导数等于该周线上的加速度环量

以上结论是纯运动学性质的，对任何流体都成立



开尔文定理3

理想流体



$$\rho \frac{D\vec{u}}{Dt} = -\nabla p + \rho \vec{f}$$

欧拉运动方程

质量力有势且为单值函数



$$\vec{f} = -\nabla G$$

$$\begin{aligned} \Rightarrow \frac{D\vec{u}}{Dt} = -\frac{\nabla p}{\rho} - \nabla G & \Rightarrow \frac{D\Gamma}{Dt} = \oint_{C(t)} -\frac{\nabla p}{\rho} \cdot d\vec{r} - \oint_{C(t)} \nabla G \cdot d\vec{r} \end{aligned}$$

正压流体



$$\rho = \rho(p)$$

- ④ 流体作等熵流动，等温流动，等密度流动等均可视为正压流体



开尔文定理4

$$\rho = \rho(p) \implies d \int \frac{dp}{\rho(p)} = \frac{dp}{\rho}$$

引入标量算符 $d\vec{r} \cdot \nabla = dx \frac{\partial}{\partial x} + dy \frac{\partial}{\partial y} + dz \frac{\partial}{\partial z} = d$

$$\implies d\vec{r} \cdot \frac{\nabla p}{\rho} = \frac{dp}{\rho} = d \int \frac{dp}{\rho(p)} = d\vec{r} \cdot \nabla \int \frac{dp}{\rho(p)}$$

由于 $d\vec{r}$ 是任取的，所以对正压流体流场中任一点

$$\implies \frac{\nabla p}{\rho} = \nabla \int \frac{dp}{\rho}$$



开尔文定理5

设理想、正压流体，质量力有势且为单值函数

$$\begin{aligned}\frac{D\Gamma}{Dt} &= \oint_{C(t)} \left(-\frac{\nabla p}{\rho} - \nabla G \right) \cdot d\vec{r} = \oint_{C(t)} \left(-\nabla \int \frac{dp}{\rho} - \nabla G \right) \cdot d\vec{r} \\ &= - \oint_{C(t)} \nabla \left(\int \frac{dp}{\rho} + G \right) \cdot d\vec{r} = - \oint_{C(t)} d \left(\int \frac{dp}{\rho} + G \right) = 0\end{aligned}$$



$$\frac{D\Gamma}{Dt} = 0$$

- ④ 对于正压、质量力单值有势的理想流体流动，沿任意封闭物质周线上的速度环量守恒



开尔文定理6

设在封闭的物质线 $C(t)$ 上张一曲面 $A(t)$ ，则由 Stokes 定理

$$\Gamma = \oint_{A(t)} \vec{\Omega} \cdot \vec{n} dA$$



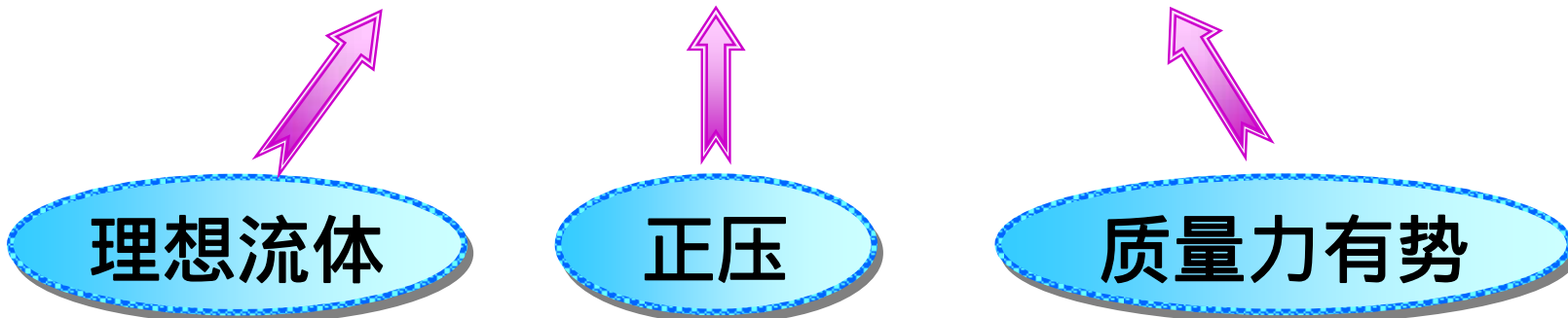
$$\frac{D\Gamma}{Dt} = \frac{D}{Dt} \oint_{A(t)} \vec{\Omega} \cdot \vec{n} dA = 0$$

- ④ 对于正压、质量力单值有势的理想流体流动，通过任意物质面的涡通量守恒



开尔文定理7

开尔文定理成立的条件



- ④ 放松任何一个条件，开尔文定理不成立
- ④ 粘性，非正压流体与质量力无势是引起速度环量和涡通量发生变化的三大因素



开尔文定理8

涡旋不生不灭定理



设流体理想、正压、质量力有势

- ① 若某时刻在某部分流体内无旋，则以前或以后任一时刻这部分流体皆无旋

$$\vec{\Omega} = 0 \xrightarrow{\text{开尔文定理}} \int_S \vec{\Omega} \cdot d\vec{S} = 0 \xrightarrow{S \text{ 任取}} \int_{S'} \vec{\Omega} \cdot d\vec{S} = 0 \xrightarrow{\text{开尔文定理}} \vec{\Omega} = 0$$

- ② 若某时刻该部分流体有旋，则以前或以后的任何时刻这部分流体皆为有旋

设任何时刻无旋 $\xrightarrow{\text{开尔文定理}}$ 一直无旋 $\xrightarrow{\text{开尔文定理}}$ 与有旋矛盾



开尔文定理9

**涡管强度
保持定理**



涡管在随流体运动过程中通过其任一横截面的涡通量，即涡管强度不随时间改变

取 $C(t)$ 是涡管横截面 $A(t)$ 上围绕涡管一周的封闭物质周线，则在某一瞬时

$$\frac{D\Gamma}{Dt} = \frac{D}{Dt} \oint_{C(t)} \vec{u} \cdot d\vec{r} = \frac{D}{Dt} \oint_{A(t)} \vec{\Omega} \cdot \vec{n} dA = 0$$

- ④ 在运动过程中涡管会发生变形：当涡管被拉伸时，涡量增大，涡管被压缩时，涡量减小，以保持通过横截面的总的涡通量不变



开尔文定理10

④ 涡量场是无源场

$$\nabla \cdot \vec{\Omega} = 0$$



$$\int_{A_1} \vec{n} \cdot \vec{\Omega} dA = \int_{A_2} \vec{n} \cdot \vec{\Omega} dA$$

- ④ 每一瞬时通过同一涡管任意截面的涡通量处处相等，即涡管强度在空间上守恒
- ④ 满足开尔文定理时，涡管强度不但具有空间上的守恒性，而且具有时间上的守恒性



3.2 伯努利方程

兰姆—葛罗米柯方程

$$(\vec{u} \cdot \nabla)\vec{u} = \nabla\left(\frac{\vec{u} \cdot \vec{u}}{2}\right) - \vec{u} \times (\nabla \times \vec{u})$$

P.393

理想流体



$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla)\vec{u} = -\frac{\nabla p}{\rho} + \vec{f}$$



$$\frac{\partial \vec{u}}{\partial t} + \nabla\left(\frac{\vec{u} \cdot \vec{u}}{2}\right) - \vec{u} \times \vec{\Omega} = -\frac{\nabla p}{\rho} + \vec{f}$$

质量力有势、正压



$$\vec{f} = -\nabla G$$

$$d \int \frac{dp}{\rho(p)} = \frac{dp}{\rho}$$



$$\frac{\partial \vec{u}}{\partial t} + \nabla\left(\frac{\vec{u} \cdot \vec{u}}{2}\right) - \vec{u} \times \vec{\Omega} = -\nabla \int \frac{dp}{\rho} - \nabla G$$



兰姆—葛罗米柯方程

$$\frac{\partial \vec{u}}{\partial t} + \nabla \left(\frac{\vec{u} \cdot \vec{u}}{2} \right) - \vec{u} \times \vec{\Omega} = -\nabla \int \frac{dp}{\rho} - \nabla G$$



$$\frac{\partial \vec{u}}{\partial t} + \nabla \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = \vec{u} \times \vec{\Omega}$$

- ④ 右侧项类似于哥氏加速度 $\vec{a}_c = 2\vec{\omega} \times \vec{u}_r$ ，与速度和流线方向垂直



伯努利方程1

沿流线的伯努利方程

定常流动

$$\frac{\partial \vec{u}}{\partial t} + \nabla \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = \vec{u} \times \vec{\Omega}$$
$$d\vec{l} \cdot \nabla = dx \frac{\partial}{\partial x} + dy \frac{\partial}{\partial y} + dz \frac{\partial}{\partial z} = d$$

$$\nabla \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = \vec{u} \times \vec{\Omega}$$

沿流线取线元 $d\vec{l}$ $d\vec{l} \cdot \nabla \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = d\vec{l} \cdot (\vec{u} \times \vec{\Omega})$

$$\Rightarrow d \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = 0 \Rightarrow \int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G = C$$

C 为伯努利常数，沿同一条流线为常数



伯努利方程2

伯努利方程或
伯努利积分



$$\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G = C$$

④ 理想流体、质量力有势、正压、定常、沿流线

不可压缩流体定常流动

$$\Rightarrow \frac{D\rho}{Dt} = \frac{\partial \rho}{\partial t} + (\vec{u} \cdot \nabla)\rho = 0 \Rightarrow (\vec{u} \cdot \nabla)\rho = 0 \quad \downarrow$$

$$\int \frac{dp}{\rho} = \frac{p}{\rho} + C_0 \quad \leftarrow \text{沿流线密度为常数}$$



伯努利方程3

质量力只有重力， z 轴铅垂向上

$$\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G = C$$

$$\vec{f} = -\nabla G = -g\vec{e}_z \quad \Longrightarrow \quad G = gz$$



$$\frac{p}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + gz = C$$

- ④ 理想不可压缩流体、质量力只有重力、重力加速度沿 z 轴负向、定常、沿流线
- ④ 单位质量流体的机械能沿一条流线守恒



伯努利方程4

理想流体非定常流动

$$\frac{\partial \vec{u}}{\partial t} + \nabla \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = \vec{u} \times \vec{\Omega}$$

沿流线取线元 dl

$$\frac{\partial \vec{u}}{\partial t} \cdot d\vec{l} + d\vec{l} \cdot \nabla \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = d\vec{l} \cdot (\vec{u} \times \vec{\Omega})$$

$$\Rightarrow \frac{\partial u}{\partial t} dl + d \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = 0$$

$$\int_1^2 \frac{\partial u}{\partial t} dl + \int_1^2 d \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = 0$$

质量力只有重力， z 轴铅垂向上，密度沿流线为常数，理想

$$\Rightarrow \frac{p_1}{\rho} + \frac{\vec{u}_1 \cdot \vec{u}_1}{2} + gz_1 = \frac{p_2}{\rho} + \frac{\vec{u}_2 \cdot \vec{u}_2}{2} + gz_2 + \int_1^2 \frac{\partial u}{\partial t} dl$$



伯努利方程5

势流伯努利方程

$$\frac{\partial \vec{u}}{\partial t} + \nabla \left(\int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = \vec{u} \times \vec{\Omega}$$

$$\vec{u} = \nabla \phi \implies \frac{\partial \vec{u}}{\partial t} = \frac{\partial(\nabla \phi)}{\partial t} = \nabla \left(\frac{\partial \phi}{\partial t} \right)$$

$$\vec{\Omega} = \mathbf{0} \implies \nabla \left(\frac{\partial \phi}{\partial t} + \int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G \right) = \mathbf{0}$$

$$\implies \frac{\partial \phi}{\partial t} + \int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G = f(t)$$

柯西—拉格朗日积分

④ $f(t)$ 是时间的函数，同一时刻在全场处处相等，称非定常伯努利常数



伯努利方程6

$$\frac{\partial \phi}{\partial t} + \int \frac{dp}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} + G = f(t)$$

④ 理想、正压、质量力有势、无旋

定常流动



$$\int \frac{dp}{\rho} + \frac{\nabla \phi \cdot \nabla \phi}{2} + G = f$$

④ f 在全场为常数，不同于沿流线的伯努利方程



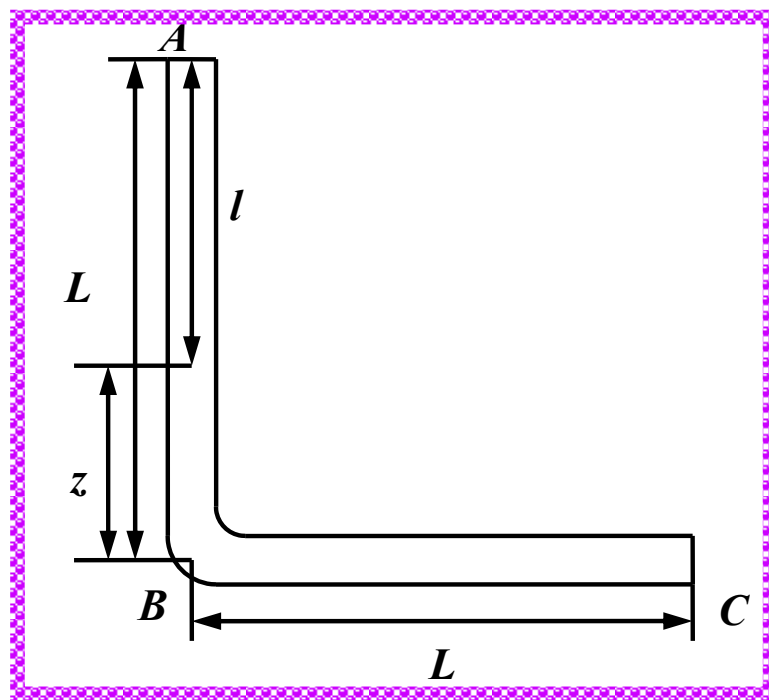
伯努利方程例题1-1

如图所示的等截面直角管道ABC，垂直段管长AB，水平段管长BC， $AB = BC = L$ ，管中盛满理想不可压缩均质的水，C处有阀门，管口接大气，大气压强为 p_a ，质量力为重力。求：当阀门突然打开，管中压强分布如何？

管道中心线可看作流线，流线从A点开始计算，由不可压连续方程

$$u = u(t)$$

同一时刻，管道中各截面速度相同，则 du/dt 也相同





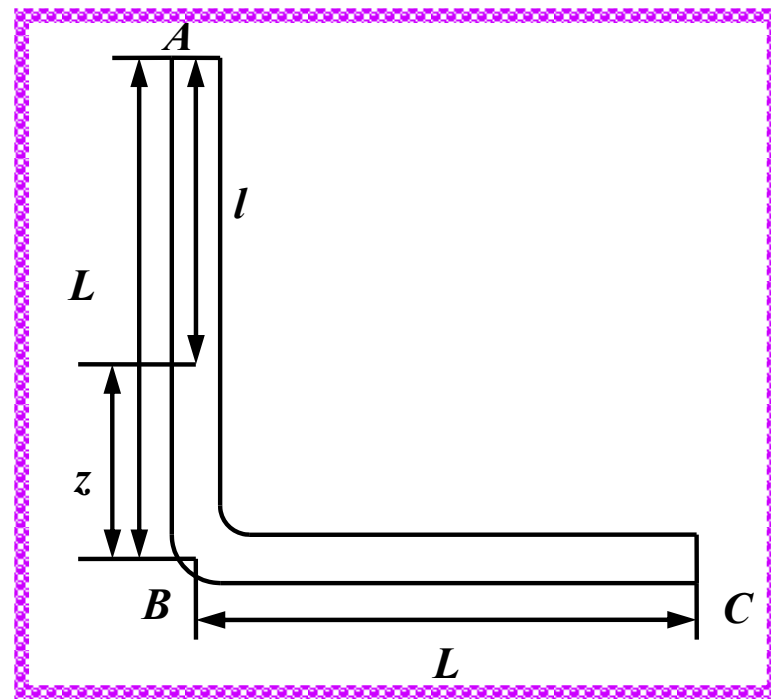
伯努利方程例题1-2

对 l 段列非定常伯努利方程

$$\frac{p_A}{\rho} + gz_A = \frac{p}{\rho} + gz + \int_0^l \frac{\partial u}{\partial t} dl$$

对A、C段列非定常伯努利方程

$$\frac{p_A}{\rho} + gz_A = \frac{p_C}{\rho} + gz_C + \int_A^C \frac{\partial u}{\partial t} dl$$



由 $p_A = p_C = p_a$ $z_A = L$, $z_C = 0$

$$\Rightarrow \frac{\partial u}{\partial t} = \frac{g}{2} \Rightarrow \frac{p}{\rho} = \frac{p_a}{\rho} + gL - gz - \frac{gl}{2}$$

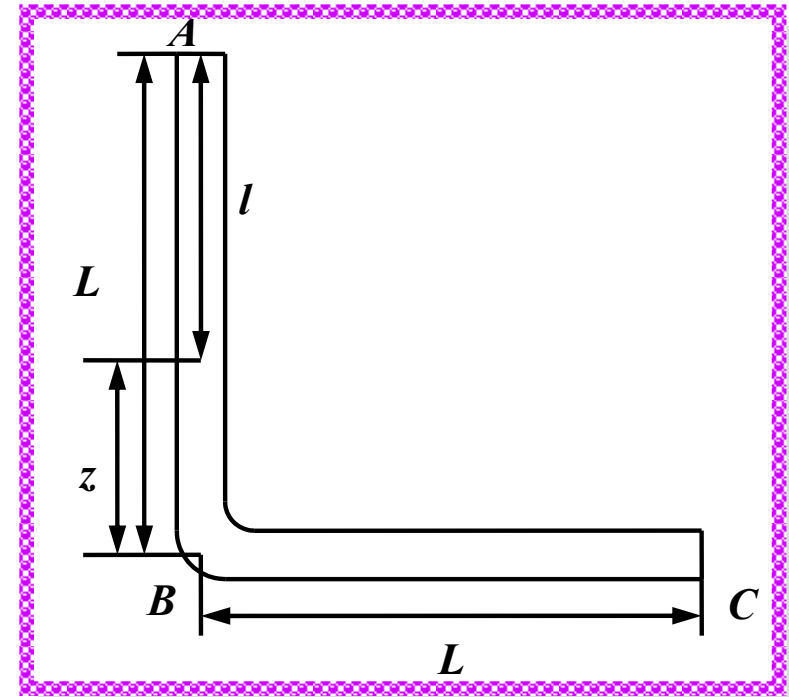
垂直管中, $l = L - z \Rightarrow \frac{p}{\rho} = \frac{p_a}{\rho} + \frac{g}{2}(L - z)$



伯努利方程例题1-3

水平管中， $l > L$ ， $z = 0$

$$\Rightarrow \frac{p}{\rho} = \frac{p_a}{\rho} + gL - \frac{gl}{2}$$





伯努利方程例题2-1

例：液体在两头开口的等横截面U型管中振荡，液柱长 L ，液面上方为大气压强 p_a ，忽略粘性摩擦力和表面张力。求液柱运动规律。初始时刻U型管两端自由面高度差为 h ，液体静止。液体密度为常数

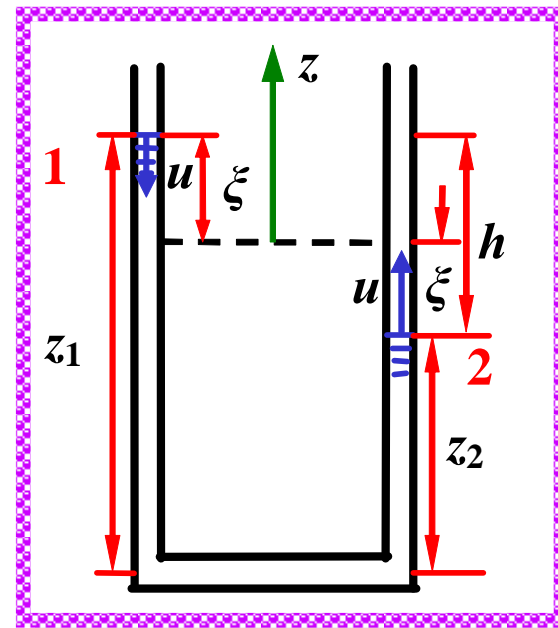
管内流动作一维流动处理，速度只是时间的函数，取速度正向由1指向

2

$$u = u(t) = -\frac{d\xi}{dt}$$

ξ 是液面至平衡位置的距离

应用非定常伯努利方程





伯努利方程例题2-2

$$\frac{p_1}{\rho} + \frac{\vec{u}_1 \cdot \vec{u}_1}{2} + gz_1 = \frac{p_2}{\rho} + \frac{\vec{u}_2 \cdot \vec{u}_2}{2} + gz_2 + \int_1^2 \frac{\partial u}{\partial t} dl$$

式中 $p_1 = p_2 = p_a$ $z_1 = \xi$ $z_2 = -\xi$ $u_1^2 = u_2^2$

→ $2g\xi = \int_1^2 \frac{\partial u}{\partial t} dl = \frac{\partial u}{\partial t} \int_1^2 dl = \frac{\partial u}{\partial t} L = -\frac{d^2 \xi}{dt^2} L$

→ $\frac{d^2 \xi}{dt^2} + \frac{2g}{L} \xi = 0$

→ $\xi = C_1 \cos\left(\sqrt{\frac{2g}{L}} t\right) + C_2 \sin\left(\sqrt{\frac{2g}{L}} t\right)$

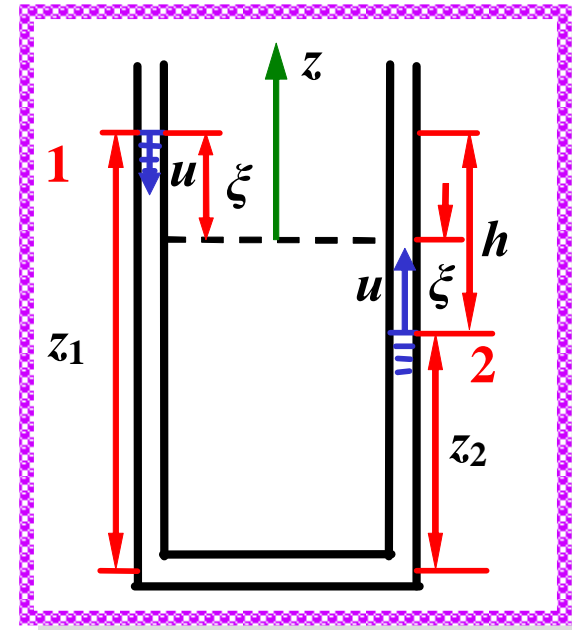


伯努利方程例题2-3

初始条件： $t = 0$ 时 $\xi = \frac{h}{2}$ $\frac{d\xi}{dt} = 0$

→ $C_1 = \frac{h}{2}$, $C_2 = 0$

→ $\xi = \frac{h}{2} \cos\left(\sqrt{\frac{2g}{L}}t\right)$



振动周期 → $2\pi\sqrt{\frac{L}{2g}}$

速度 → $u = -\frac{d\xi}{dt} = \frac{h}{2}\sqrt{\frac{2g}{L}}\sin\left(\sqrt{\frac{2g}{L}}t\right)$



伯努利方程例题3-1

例：在原静止的理想无界均质不可压缩流体中有一半半径为 a 的气球，初始时刻气球内部表压强为 p_0 ，气球表面的速度为零，若不考虑质量力和表面张力的作用，且设无穷远处的压强为零，试在等温条件下确定气球半径随时间的变化规律

取球坐标系，坐标原点在球心，流体只有径向运动，物理量只是 r 和 t 的函数，考虑流场中任意球面，半径为 r ，速度为 u_r ，根据连续方程

$$4\pi r^2 u_r = f(t)$$

设气球表面半径为 R ，气球表面法向速度为 \dot{R}



$$4\pi r^2 u_r = 4\pi R^2 \dot{R} \quad r > R$$



伯努利方程例题3-2

$$\Rightarrow u_r = \frac{R^2 \dot{R}}{r^2} = \frac{\partial \phi}{\partial r}$$

$$\Rightarrow \phi = -\frac{R^2 \dot{R}}{r} \quad \text{取无穷远处速度势函数为零}$$

对气球附近和无穷远处列势流伯努利方程，取无穷远处表压为零

$$\Rightarrow \frac{\partial \phi}{\partial t} + \frac{p}{\rho} + \frac{\vec{u} \cdot \vec{u}}{2} = 0$$

$$\text{由} \quad \frac{\partial \phi}{\partial t} = -\frac{1}{r} (2R\dot{R}\dot{R} + R^2\ddot{R}) \quad \vec{u} \cdot \vec{u} = \frac{R^4 \dot{R}^2}{r^4}$$

$$\Rightarrow -\frac{1}{r} (2R\dot{R}\dot{R} + R^2\ddot{R}) + \frac{R^4 \dot{R}^2}{2r^4} + \frac{p}{\rho} = 0$$



伯努利方程例题3-3

令 $r = R \implies R\ddot{R} + \frac{3}{2}\dot{R}^2 = \frac{p_b}{\rho}$ p_b 是球面压强

气球运动过程是等温的，且 $R = a$ 时， $p = p_0$

$$p_b R^3 = p_0 a^3 \implies R\ddot{R} + \frac{3}{2}\dot{R}^2 = \frac{p_0}{\rho} \left(\frac{a}{R}\right)^3$$

两边乘以 $2R^2\dot{R} \implies 2R^3\dot{R}\ddot{R} + 3R^2\dot{R}^3 = \frac{2p_0 a^3}{\rho} \frac{\dot{R}}{R}$

由 $2R^3\dot{R}\ddot{R} + 3R^2\dot{R}^3 = \frac{d}{dt}(R^3\dot{R}^2) \implies \frac{d}{dt}(R^3\dot{R}^2) = \frac{2p_0 a^3}{\rho} \frac{\dot{R}}{R}$



伯努利方程例题3-4

积分一次 $\xrightarrow{R=a \text{ 时 } \dot{R}=0}$ $R^3 \dot{R}^2 = \frac{2p_0 a^3}{\rho} \ln \frac{R}{a}$

再积分一次 \Rightarrow $t = \frac{1}{\sqrt{\frac{2p_0 a^3}{\rho}}} \int_a^R \frac{R^{3/2} dR}{\sqrt{\ln \frac{R}{a}}}$



3.4 涡量动力学方程

流体密度和粘性系数均为常数

动量方程为
$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = -\frac{\nabla p}{\rho} + \nu \nabla^2 \vec{u} + \vec{f}$$

由矢量恒等式 P.393 $\implies (\vec{u} \cdot \nabla) \vec{u} = \frac{1}{2} \nabla(\vec{u} \cdot \vec{u}) - \vec{u} \times (\nabla \times \vec{u})$

$\implies \frac{\partial \vec{u}}{\partial t} + \frac{1}{2} \nabla(\vec{u} \cdot \vec{u}) - \vec{u} \times \vec{\Omega} = -\frac{\nabla p}{\rho} + \nu \nabla^2 \vec{u} - \nabla G$

对上式两边取旋度 \Downarrow

$$\nabla \times \left(\frac{\partial \vec{u}}{\partial t} \right) + \cancel{\nabla \times \nabla \left(\frac{\vec{u} \cdot \vec{u}}{2} \right)} - \nabla \times (\vec{u} \times \vec{\Omega}) = -\cancel{\nabla \times \nabla \left(\frac{p}{\rho} \right)} + \nabla \times (\nu \nabla^2 \vec{u}) - \cancel{\nabla \times \nabla G}$$



涡量动力学方程2

$$\nabla \times \left(\frac{\partial \vec{u}}{\partial t} \right) - \nabla \times (\vec{u} \times \vec{\Omega}) = \nabla \times (\nu \nabla^2 \vec{u})$$

→
$$\frac{\partial \vec{\Omega}}{\partial t} - \nabla \times (\vec{u} \times \vec{\Omega}) = \nu \nabla^2 \vec{\Omega}$$

由矢量恒等式

$$\nabla \times (\vec{u} \times \vec{\Omega}) = \vec{u} \times (\nabla \cdot \vec{\Omega}) - \vec{\Omega} \times (\nabla \cdot \vec{u}) - (\vec{u} \cdot \nabla) \vec{\Omega} + (\vec{\Omega} \cdot \nabla) \vec{u}$$

涡量场是无源场，不可压流体速度场是无源场

→
$$\frac{\partial \vec{\Omega}}{\partial t} + (\vec{u} \cdot \nabla) \vec{\Omega} = (\vec{\Omega} \cdot \nabla) \vec{u} + \nu \nabla^2 \vec{\Omega} = \frac{D\vec{\Omega}}{Dt}$$



涡量动力学方程3

$$\frac{D\vec{\Omega}}{Dt} = \frac{\partial\vec{\Omega}}{\partial t} + (\vec{u} \cdot \nabla)\vec{\Omega} = (\vec{\Omega} \cdot \nabla)\vec{u} + \nu\nabla^2\vec{\Omega}$$

④ 均质不可压缩流体、质量力有势、粘性系数为常数

$$\frac{D\vec{\Omega}}{Dt} = \frac{\partial\vec{\Omega}}{\partial t} + (\vec{u} \cdot \nabla)\vec{\Omega} \quad \Rightarrow \quad \text{涡量的随体导数，第一项是当地导数，第二项是对流导数}$$

$$\nu\nabla^2\vec{\Omega} \quad \Rightarrow$$

粘性对涡量变化的影响主要是粘性扩散，运动粘性系数在这里相当于扩散系数。扩散的作用是抹平差距，直至全流场涡量强度相等为止



涡量动力学方程4

涡量矢量 $\vec{\Omega}$ 与涡线相切，设涡线方向为 l ，则

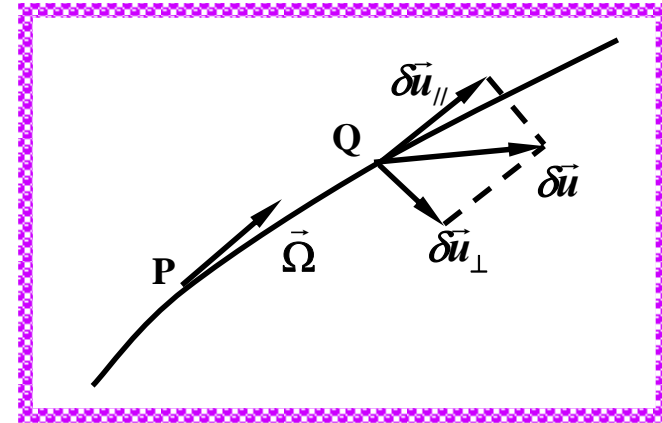
$$\Omega_l = |\vec{\Omega}|$$

$$\Rightarrow (\vec{\Omega} \cdot \nabla) \vec{u} = \Omega_l \frac{\partial \vec{u}}{\partial l} = |\vec{\Omega}| \lim_{PQ \rightarrow 0} \frac{\delta \vec{u}}{PQ}$$

$$= |\vec{\Omega}| \lim_{PQ \rightarrow 0} \frac{\delta \vec{u}_{//}}{PQ} + |\vec{\Omega}| \lim_{PQ \rightarrow 0} \frac{\delta \vec{u}_{\perp}}{PQ}$$

使涡线拉伸或压缩

使涡线扭曲



- 使涡线拉伸或压缩，或而使涡线扭曲，结果都会导致涡量的变化



涡量动力学方程5

涡量方程中没有压强 p 出现，可在压强场未知情况下求解速度场和涡量场，再确定压强场

$$\frac{\partial \vec{u}}{\partial t} + (\vec{u} \cdot \nabla) \vec{u} = -\frac{\nabla p}{\rho} + \nu \nabla^2 \vec{u}$$

两边取散度 $\nabla \cdot \frac{\partial \vec{u}}{\partial t} + \nabla \cdot [(\vec{u} \cdot \nabla) \vec{u}] = -\nabla \cdot \nabla \left(\frac{p}{\rho} \right) + \nu \nabla \cdot \nabla^2 \vec{u}$



$$\nabla \cdot [(\vec{u} \cdot \nabla) \vec{u}] = -\nabla \cdot \nabla \left(\frac{p}{\rho} \right)$$

由矢量恒等式 $(\vec{u} \cdot \nabla) \vec{u} = \frac{1}{2} \nabla^2 (\vec{u} \cdot \vec{u}) - \nabla \cdot [\vec{u} \times (\nabla \times \vec{u})]$



涡量动力学方程6

$$\nabla \cdot [\vec{u} \times (\nabla \times \vec{u})] = \nabla \cdot [\vec{u} \times \vec{\Omega}] = \vec{\Omega} \cdot (\nabla \times \vec{u}) - \vec{u} \cdot (\nabla \times \vec{\Omega})$$

$$\nabla \times \vec{\Omega} = \nabla \times (\nabla \times \vec{u}) = \nabla(\nabla \cdot \vec{u}) - \nabla^2 \vec{u} = -\nabla^2 \vec{u}$$

$$\Rightarrow \nabla \cdot [\vec{u} \times (\nabla \times \vec{u})] = \vec{\Omega} \cdot (\nabla \times \vec{u}) + \vec{u} \cdot (\nabla^2 \vec{u})$$

$$\Rightarrow \nabla \cdot [(\vec{u} \cdot \nabla) \vec{u}] = \frac{1}{2} \nabla^2 (\vec{u} \cdot \vec{u}) - \vec{\Omega} \cdot \vec{\Omega} - \vec{u} \cdot (\nabla^2 \vec{u}) = -\nabla \cdot \nabla \left(\frac{p}{\rho} \right)$$

$$\Rightarrow \nabla^2 \left(\frac{p}{\rho} \right) = \vec{\Omega} \cdot \vec{\Omega} + \vec{u} \cdot (\nabla^2 \vec{u}) - \frac{1}{2} \nabla^2 (\vec{u} \cdot \vec{u})$$

获得了涡量场和速度场后可根据上式求解压强场



涡量动力学方程7

理想流体

$$\frac{D\vec{\Omega}}{Dt} = \frac{\partial\vec{\Omega}}{\partial t} + (\vec{u} \cdot \nabla)\vec{\Omega} = (\vec{\Omega} \cdot \nabla)\vec{u} + \nu\nabla^2\vec{\Omega}$$



$$\frac{\partial\vec{\Omega}}{\partial t} + (\vec{u} \cdot \nabla)\vec{\Omega} = (\vec{\Omega} \cdot \nabla)\vec{u}$$



涡量方程例题1

例：证明在有势外力场作用下理想不可压缩均质流体满足下列方程：(1) 平面流动时 $D\vec{\Omega}/Dt = 0$ ；

(2) 轴对称流动时， $\frac{D}{Dt}\left(\frac{\vec{\Omega}}{R}\right) = 0$ 其中 R 是空间点到对称轴的距离

证明：(1) 设运动平面为xoy平面，则

$$\Omega_z = \frac{\partial v}{\partial x} - \frac{\partial u}{\partial y} \neq 0 \quad \Omega_x = \Omega_y = 0$$

由理想流体涡量方程 $\frac{D\vec{\Omega}}{Dt} = (\vec{\Omega} \cdot \nabla)\vec{u}$

$$\Rightarrow (\vec{\Omega} \cdot \nabla)\vec{u} = \Omega_z \frac{\partial \vec{u}}{\partial z} = \Omega_z \frac{\partial}{\partial z} (u\vec{i} + v\vec{j}) = 0 \Rightarrow \underline{\underline{\frac{D\vec{\Omega}}{Dt} = 0}}$$



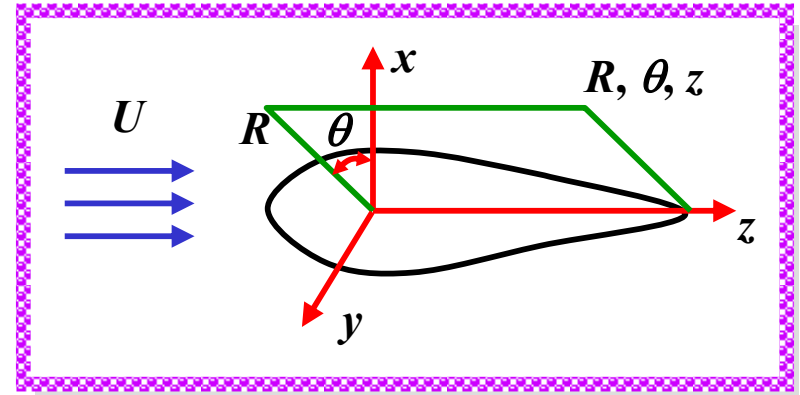
涡量方程例题2

$$\frac{D\vec{\Omega}}{Dt} = 0$$



平面流动中，涡线不会拉伸或扭曲，没有因为涡线拉伸或扭曲导致的涡量变化，对于理想流体，与流体质点固连的涡量矢量保持不变

(2) z 沿流动方向，通过 z 轴任意平面内的流动是相同的，称为轴对称流动，取圆柱坐标系， z 沿对称轴



$$u_\theta = 0, \frac{\partial}{\partial \theta} = 0$$

$$\vec{\Omega} = \frac{1}{R} \begin{vmatrix} \vec{e}_R & R\vec{e}_\theta & \vec{e}_z \\ \frac{\partial}{\partial R} & \frac{\partial}{\partial \theta} & \frac{\partial}{\partial z} \\ u_R & Ru_\theta & u_z \end{vmatrix} = \left(\frac{\partial u_R}{\partial z} - \frac{\partial u_z}{\partial R} \right) \vec{e}_\theta = \Omega_\theta \vec{e}_\theta \quad \text{P.404}$$

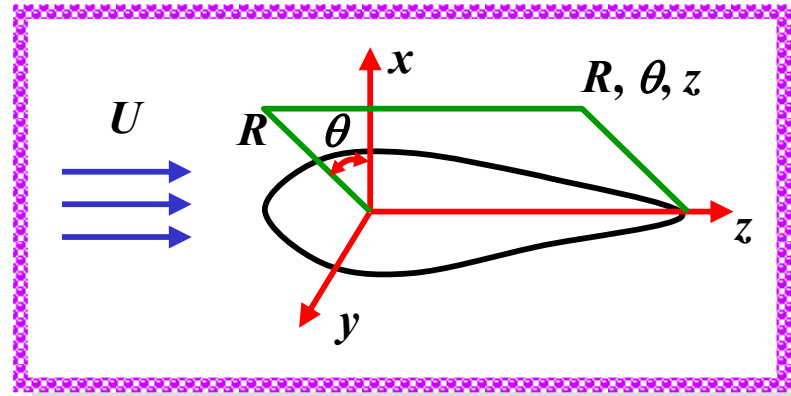


涡量方程例题3

涡量只有 θ 方向分量，与流动平面垂直

$$(\vec{\Omega} \cdot \nabla) \vec{u} = \frac{\Omega_\theta}{R} \frac{\partial \vec{u}}{\partial \theta} = \frac{\Omega_\theta}{R} \frac{\partial}{\partial \theta} (u_R \vec{e}_R + u_z \vec{e}_z) \quad \text{P.404}$$

$$= \frac{\Omega_\theta}{R} u_R \frac{\partial \vec{e}_R}{\partial \theta} = \frac{\Omega_\theta}{R} u_R \vec{e}_\theta = \frac{\vec{\Omega}}{R} u_R$$



由理想流体涡量方程

$$\frac{D\vec{\Omega}}{Dt} = (\vec{\Omega} \cdot \nabla) \vec{u}$$

$$\Rightarrow \frac{D\vec{\Omega}}{Dt} - \frac{\vec{\Omega}}{R} u_R = 0 \quad \Rightarrow \quad \frac{1}{R} \frac{D\vec{\Omega}}{Dt} - \frac{\vec{\Omega}}{R^2} u_R = 0$$



涡量方程例题4



$$\underline{\underline{\frac{D}{Dt} \left(\frac{\vec{\Omega}}{R} \right) = 0}}$$

环绕对称轴，长为 $2\pi R$ 的环形涡线，当 R 变化时涡线被拉伸或压缩， Ω 会相应增加或减小，而 Ω/R 则保持不变



作业

作业：P.84 ~ 86

④ 3.1

④ 3.6

④ 3.9

④ 3.10